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A FAST BOUNDARY TRACKING ALGORITHM FOR CONSTRAINED NONLINEAR MA--ETC(U)

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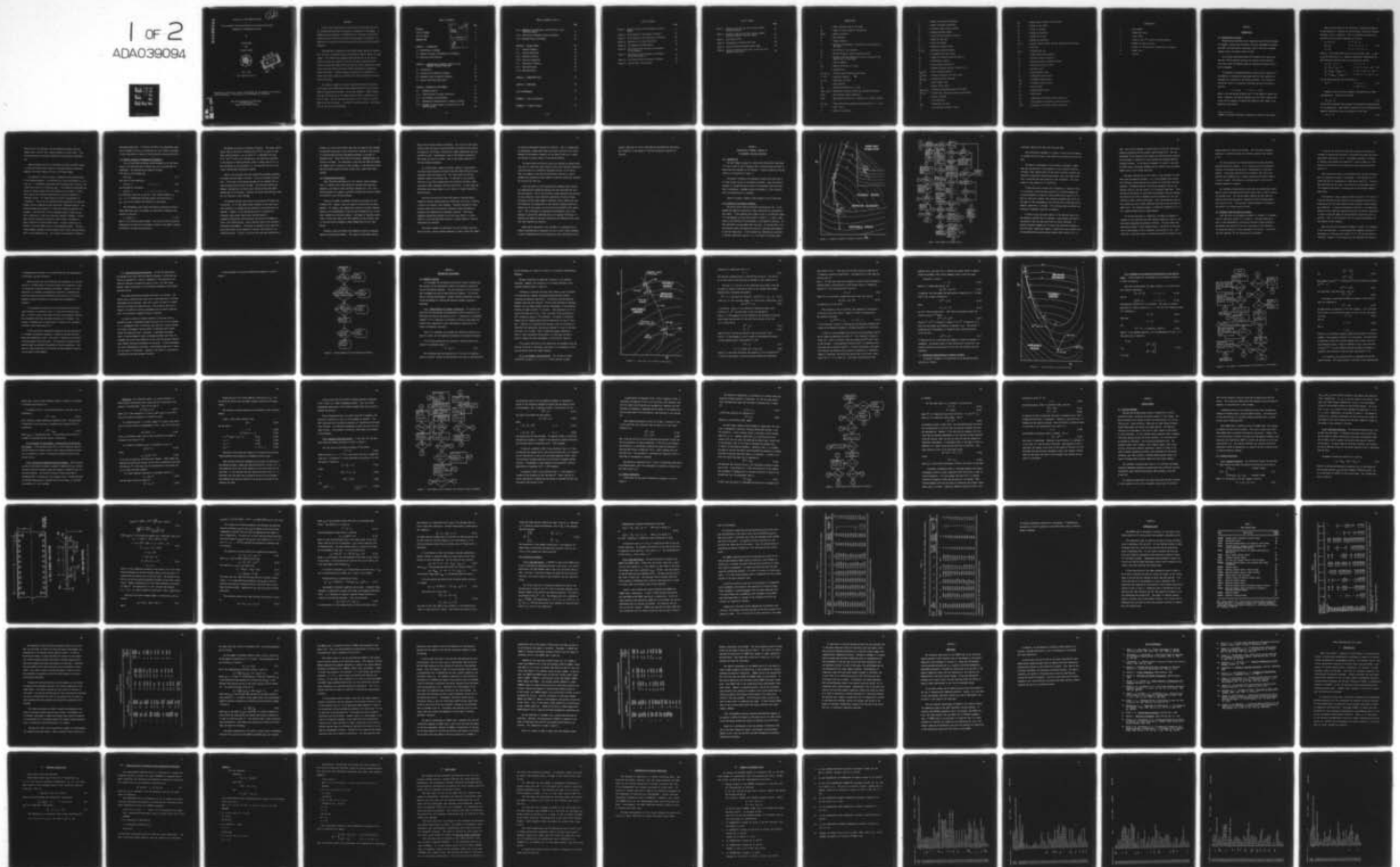
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Contract No. ONR N00014-75-C0987

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A Fast Boundary Tracking Algorithm for Constrained Nonlinear  
Mathematical Programming Problems

by

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and

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March 1977

NJIT Report No. NV 12



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## ABSTRACT

A fast search algorithm for the solution of nonlinear mathematical programming optimization problems is presented in this Report. A gradient search procedure is combined with a "Boundary Tracking"(BT) method using the feasible direction finding method of Zoutendijk for generating a feasible starting direction along the feasible-infeasible boundary.

The algorithm is applied to the minimum weight design of submersible, circular, cylindrical shells reinforced by equally spaced "T" type frames. This problem had produced algorithm failure in two earlier studies and was only recently solved by the Direct Search-Feasible Direction Algorithm (DSFD) which was shown by recent comparison studies to be among the fastest and most reliable mathematical programming methods available. The BT procedure was found to be substantially faster than DSFD, producing a solution with about one-eighth the effort required by DSFD.

In a general comparison study a code based on the BT algorithm was compared with twenty other codes representing most of the popular numerical optimization methods on ten test problems. These problems are such that majority of the codes tested failed to solve more than half of them. The new code proved superior to all others in overall generality and efficiency. It solved all problems and was the fastest code on the constrained problems.

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# NOMENCLATURE

$A$	= cross sectional area of the frame
$A_j$	= number of active behavior constraints
$B_k(x)$	= behavior function
$b$	= web thickness
$b'$	= flange thickness
$c$	= distance from midplane of the shell to the surface of the frame
$C_1$	= an arbitrary large constant
$C_2$	= maximum flange to plating thickness ratio
$d$	= distance from the midplane of the hull plating to the neutral axis of the frame
$E$	= tensile modulus
$EI_f$	= bending stiffness of a frame
$e$	= eccentricity
$e_1, e_2, e_3$	= arbitrary small positive constraints
$f, f(x)$	= objective function
$f_a, \bar{f}_a$	= efficiency criteria
$G$	= shear modulus
$GJ_f$	= torsional stiffness of a frame
$g(x), g_j(x)$	= constraint function and the $j$ th constraint function
$g^*(x)$	= the smallest proper constraint
$g(t)$	= the constraint $g^*(x)$ as a function of a single variable $t$
$H_E, H_M$	= frame deflection parameters [see equations 3.11 - 3.12]
$h$	= web height
$I$	= number of variables

$J$	= number of constraint equations
$K$	= number of proper constraints
$k_j$	= arbitrary small positive number
$L'$	= distance between frames
$L_k$	= lower limit on behavior function
$L_s$	= length of the shell
$m$	= axial wave number
$N_a$	= numerical success rating
$N_1, N_2$	= arbitrary selected numbers
$n$	= circumferential wave number
$n_a$	= number of problems solved by code "a"
$p$	= hydrostatic pressure
$P_k$	= set of proper constraints
$P$	= progress towards solution (section 4.2)
$p_{cg}(n,m)$	= gross collapse pressure
$p_{cs}(n,m)$	= collapse pressure of a shell panel
$p_{cg}^*, p_{cs}^*$	= minimum collapse pressures
$Q_p$	= total radial load
$R$	= radius of the shell
$R_{min}, R_{max}$	= minimum and maximum radius of the shell
$R_i^+, R_i^-$	= active lower and upper regional constraints
$S_j$	= factor of safety
$t$	= skin thickness
$t_{ap}$	= normalized cpu time
$u$	= best movement direction vector

$V_D$	= displacement volume of the cylinder
$V_f$	= volume of the frame
$V_s$	= volume of plating
$V_w$	= volume of frame web
$W$	= weight of the hull
$W_j$	= deflection parameter
$x, x_i$	= design variable vector and its components respectively
$\alpha$	= step size
$\alpha_{\min}$	= minimum step size
$\Gamma$	= frame deflection parameter
$\gamma_s$	= specific weight of material
$\gamma_w$	= specific weight of immersion fluid
$\epsilon_j$	= constraint activity limit
$\mu$	= poisson's ratio
$\sigma_b$	= frame bending stress
$\sigma_c$	= compressive hoop stress
$\sigma_{fa}$	= allowable frame stress
$\sigma_{pa}$	= allowable plating stress
$\sigma_r$	= axial stress
$\sigma_t$	= maximum frame stress
$\sigma_\phi$	= hoop stress
$ \phi $	= magnitude of arbitrary vector function $\phi$
$\nabla\phi$	= the gradient of arbitrary vector function $\phi$
$(\phi)^T$	= transpose of arbitrary vector function $\phi$

## SUPERSCRIPTS

b	= base number
ℓ	= comparison value
L	= Lower limit
n	= value at the $n^{\text{th}}$ direction finding problem
r	= number of redesign cycles
s	= number of iterations for locating the IF boundary
U	= upper limit
0	= initial



## CHAPTER 1

### INTRODUCTION

#### 1.1 Optimization in Design

Optimal design problems may be treated by many different methods, for example, ordinary and variational calculus, mathematical programming (MP), and some special techniques, such as the fully stressed concept used in structural design [1-10]<sup>1</sup>.

Of the above mentioned methods, MP procedures [11] seem to be the most flexible methods available for optimal design synthesis since they treat the broadest range of engineering problems and are easily adaptable.

The concept of design optimization requires that a quantity to be minimized or maximized be designated and that this quantity be expressed as a function of the design variables. This function is called the "merit" or "objective" function, and can be written in the form

$$f = f(x_i) \quad i = 1, 2, \dots, I \quad (1-1)$$

where  $x_i$  are the design variables and  $I$  is the number of design variables. Generally, the design variables are not free to take on any value, but are subject to constraints governing their range or the behavior of the design.

---

<sup>1</sup>Numbers in brackets designate references at the end of the thesis.



When limits on behavior are specified, a quantitative measure of the behavior as a function of the variables, called the "behavior function",  $B(x_i)$  is required. Thus, if  $K$  behavior functions are specified, one can write  $K$  equations of the form

$$\begin{aligned} L_k &\leq B_k \leq U_k & k &= 1, 2, \dots, m \\ B_k &\leq U_k & k &= m+1, m+2, \dots, n \\ L_k &\leq B_k & k &= n+1, n+2, \dots, p \end{aligned} \quad (1.2)$$

where  $L_k$  is the lower bound on  $B_k$ , and  $U_k$  the upper limit.  $L_k$  and  $U_k$  may be functions of  $x_i$ . Behavior constraints representing the above behavior function limits can be written as follows

$$\begin{aligned} g_j &= U_j - B_j \geq 0 & j &= 1, 2, \dots, m \\ g_j &= B_{j-m} - L_{j-m} \geq 0 & j &= m+1, m+2, \dots, 2m \\ g_j &= U_{j-2m} - B_{j-2m} \geq 0 & j &= 2m+1, 2m+2, \dots, 2m+n \\ g_j &= B_{j-2m+n} - L_{j-2m+n} \geq 0 & j &= 2m+n+1, \dots, 2m+n+p \end{aligned} \quad (1.3)$$

All the above equations may be written as

$$\begin{aligned} g_j &\geq 0 & j &= 1, 2, \dots, J \\ J &= 2m + n + p \end{aligned} \quad (1.4)$$

Regional limits are often imposed by manufacturing or other considerations. These are of the form

$$x_i^L \leq x_i \leq x_i^U \quad (1.5)$$

$x_i^L$  and  $x_i^U$  are constants and represent the minimum and maximum values of  $x_i$  respectively. Here regional constraints are distinguished from behavior constraints since any constraint of the form

$$A \leq x_i \leq B \quad (1.6)$$

where  $A$  and  $B$  are constants, may be treated more simply than the general form. Not all the  $x_i$  need be subject to such limits. A detailed discussion of regional constraints can be found in Reference [9].

Some variables may also be restricted to certain discrete values. In structural design these values can represent material properties, geometric available shapes and sizes, or thickness gages.

The concept of a merit surface is important to the understanding of the redesign process. The function  $f(x_i)$  can be considered as a surface in  $I + 1$  dimensional space where the coordinate axes are the  $x_i$  and  $y$  where the value of  $y$  is given by  $f(x_i)$ . The constraints delineate the region of interest within which the optimum is to be found. Points which satisfy the constraint equations are called "acceptable" or "feasible" points. All other points are called "unacceptable" or "infeasible". The set of all feasible points constitute the "feasible region" and all infeasible points define the "infeasible region". The surface between these regions is called the Infeasible-Feasible (IF) boundary. Those portions of the IF boundary where at least one behavior constraint is zero are called the "behavior" boundary. Points away from the constraint surface are called "free", and those on these surfaces are called "bound" points. The merit surface is explored to find the highest point in the acceptable region. The algorithms commonly employed in such problems usually start the exploration from a free acceptable point. The variables are generally treated as

continuous quantities. If discrete variables are encountered, they may be treated initially as continuous and, upon finding an optimum, a local exploration is made to find the optimal discrete value [12].

### 1.2 General Strategy of Mathematical Programming

Like all optimization methods the MP methods try to find those values  $x$  for which the merit function  $f(x_i)$  will be minimized (or maximized). The problem may be stated as follows:

Find those  $x_i$  that produce the

$$\min. f(x_i) \quad (1.7)$$

such that all the constraints

$$g_j(x_i) \geq 0 \quad j = 1, 2, \dots, J \quad (1.8)$$

and the equality constraints

$$g_k(x_i) = 0 \quad k = J + 1, J + 2, \dots, K \quad (1.9)$$

are satisfied, where the  $x_i$  are the  $I$  real valued variables  $x_1, x_2, \dots, x_I$  in  $I$ -dimensional Euclidian space, and constraints  $g_1, g_2, \dots, g_K$  are real-valued real functions in that space.

Most MP methods do not treat the equality constraints directly. These constraints may, for example, be converted to inequality constraints of the form

$$\epsilon \leq g_k(x_i) \leq \epsilon \quad (1.10)$$

where  $\epsilon$  is an arbitrary small number. One can also treat an equality constraint by solving for one variable in terms of the others, thereby eliminating a variable and constraint.



MP methods are based on searching strategies. The search usually starts from an arbitrarily selected point  $x^0$  and, by means of some local search strategy, a set of points  $x^r$  is generated such that  $f(x^r) < f(x^{r-1})$  while also satisfying all the constraint equations. In the majority of design problems, either  $f$  and/or some or all of the constraints  $g_j$  are nonlinear in  $x$ , and therefore one has a nonlinear, constrained optimization problem.

None of the available nonlinear optimization methods guarantees an optimal solution (when it exists). There are two major difficulties. First, many of the design problems are not unimodal that is, they have more than one local optimum. The nonlinear methods are, however, designed only to locate local optima and thus the global optimum may not be attained. Secondly the search algorithm may simply fail to find even a local optimum.

The prudent designer thus usually tries several different starting points. If all the search paths terminate at the same point, then optimality is assumed and the problem can be considered to be unimodal. However, if the termination point is different for different search paths, then either the best design is accepted or additional starting points are tried in an attempt to find a still better design. Such a decision draws on the designer's experience and judgment. The failure to converge to the same point may be due either to the presence of several local optima, or to algorithm failure. Failure is said to occur when the algorithm ter-

minates at a point significantly away from the nearest local optimum. An excellent discussion of the difficulties involved in the solution of unconstrained nonlinear programming problems is provided in Reference [12]. These difficulties are greatly compounded when constraints are added. For convenience, since this and other MP methods are capable only of locating a local optimum, in the discussion below the term optimum should be taken to mean local rather than global optimum.

### 1.3 Motivation and Structure

Many efficient algorithms exist for treating linear problems, that is, problems with linear objective functions and constraint equations, and certain simple nonlinear problems [5-7, 13]. Most design problems are, however, nonlinear problems that must be treated by relatively less efficient methods.

There are a number of methods available for solution of such problems [14]. However, there are several difficulties with these methods. For example, the computations required to produce improved designs in the neighborhood of the constraint boundaries are in some cases lengthy and relatively complex. The number of function evaluations is often very large, and, most methods are not reliable, that is, the best points produced by these methods may not be a local optima.

Recently, Eason and Fenton [15] compared a group of seventeen numerical optimization methods. This group of algorithms contains



most of the currently popular procedures. The results of this study indicate that the direct search algorithms are superior with respect to generality, efficiency, running cost, speed, preparation cost and reliability [15]. Unfortunately, none of the methods presented in this study are totally reliable. None of the codes solved all of the ten problems attempted.

In a recent paper, Pappas and Moradi compared a code based on the Direct Search-Feasible Direction Algorithm (DSFD) [16] with those studied by Eason and Fenton [17]. This code solved all the test problems treated in Reference [15]. In addition it also solved a difficult six-variable problem which the relatively reliable DSDA, and popular SUMT, procedures failed to solve [17]. In this study the DSFD based code proved superior to all others in overall generality and efficiency.

Even the relatively efficient DSFD however, required several hundred to several thousand function evaluations to achieve a solution to Eason's and Fenton's test problems. Therefore substantial computational effort and cost would be required by these procedures on problems with computationally demanding functions. Since many important engineering problems are of this type, there is a clear need for a new algorithm which requires a reduced number of function evaluations for solution.

This thesis presents an apparently fast and reliable algorithm which utilizes a search strategy designed to greatly reduce the number

of function evaluations required for solution. This is accomplished by developing a scheme which keeps the search confined to the neighborhood of the behavior boundary, on the premise that this is where the optimum is usually found in constrained problems.

The search moves efficiently along this boundary by making effective use of a relatively small amount of new local function information relying primarily on information generated earlier in the search. Thus, the number of new function evaluations required to sustain movement and thereby the total number of function evaluations required for solution are kept low.

Since the advent of high speed digital computers many accurate but computationally demanding methods have been developed for engineering analysis. Due to the relatively large execution time required for each reanalysis cycle (function evaluation) of many of these techniques and the large number of reanalysis cycles required by most MP procedures, the combination of such analytic methods and MP procedures may be very costly to utilize and are therefore often impractical. This difficulty can seemingly be minimized by use of the Boundary Tracking (BT) algorithm due to its apparent efficiency in reducing the number of function evaluations and therefore total execution time required for solution.

Where the BT algorithm is not available in a compiled form, a simpler algorithm may be preferable for use on small simple problems. In such circumstances the extra compilation time required due to the

greater complexity of the BT algorithm may overshadow the time saved by a reduction in the number of function evaluations required for solution.

CHAPTER 2  
DESCRIPTION OF GENERAL STRATEGY OF  
THE BOUNDARY TRACKING ALGORITHM

2.1 Introduction

The most common strategy for constrained optimization techniques is first to move to the IF boundary from a starting point and then to move along this boundary to the optimum. A typical objective function surface is illustrated in Figure 1.

The general strategy of the Boundary Tracking (BT) algorithm is to first locate a point on the behavior boundary. Once the behavior boundary is located the best direction for movement along this boundary is determined. Movement along this boundary is then continued until the optimum point is obtained.

Figure 2 presents a general block diagram of the BT algorithm.

2.2 Location of the Behavior Boundary

The search starts from an arbitrary starting point  $x_i^0$ . If the problem has behavior constraints, these constraints are evaluated at this point. If the starting point proves to be in the feasible region, it is designated as a base point (point 1 Figure 1). A step is then taken in the direction of the gradient of the objective function. All the constraints are evaluated after the step. If the new point is in the feasible region the objective function is evaluated and compared to the last base point. If the function has improved, this new point is called a base point (points 2, 3, 4 in Figure 1) and the search



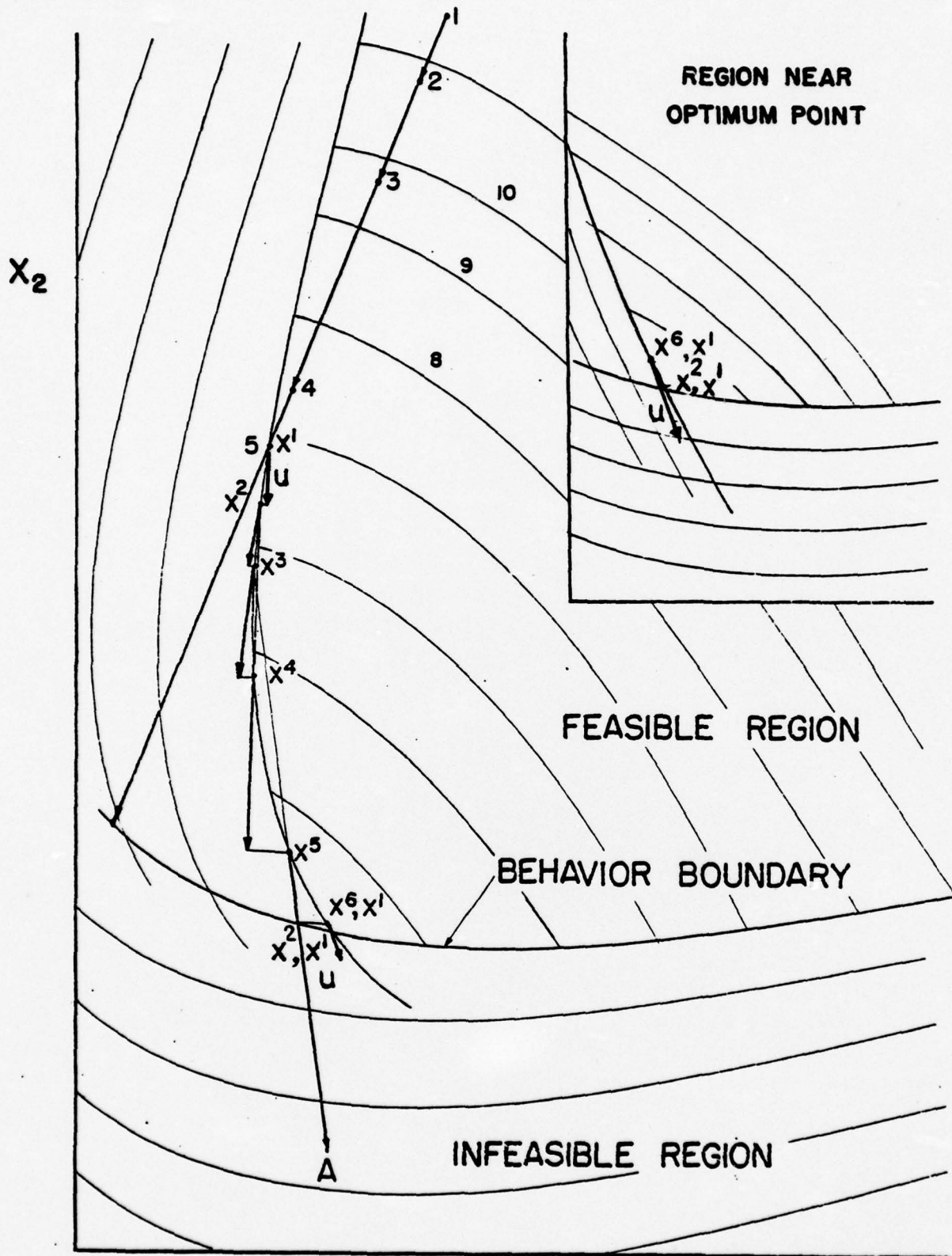


Figure 1. General Strategy of Boundary Tracking Method



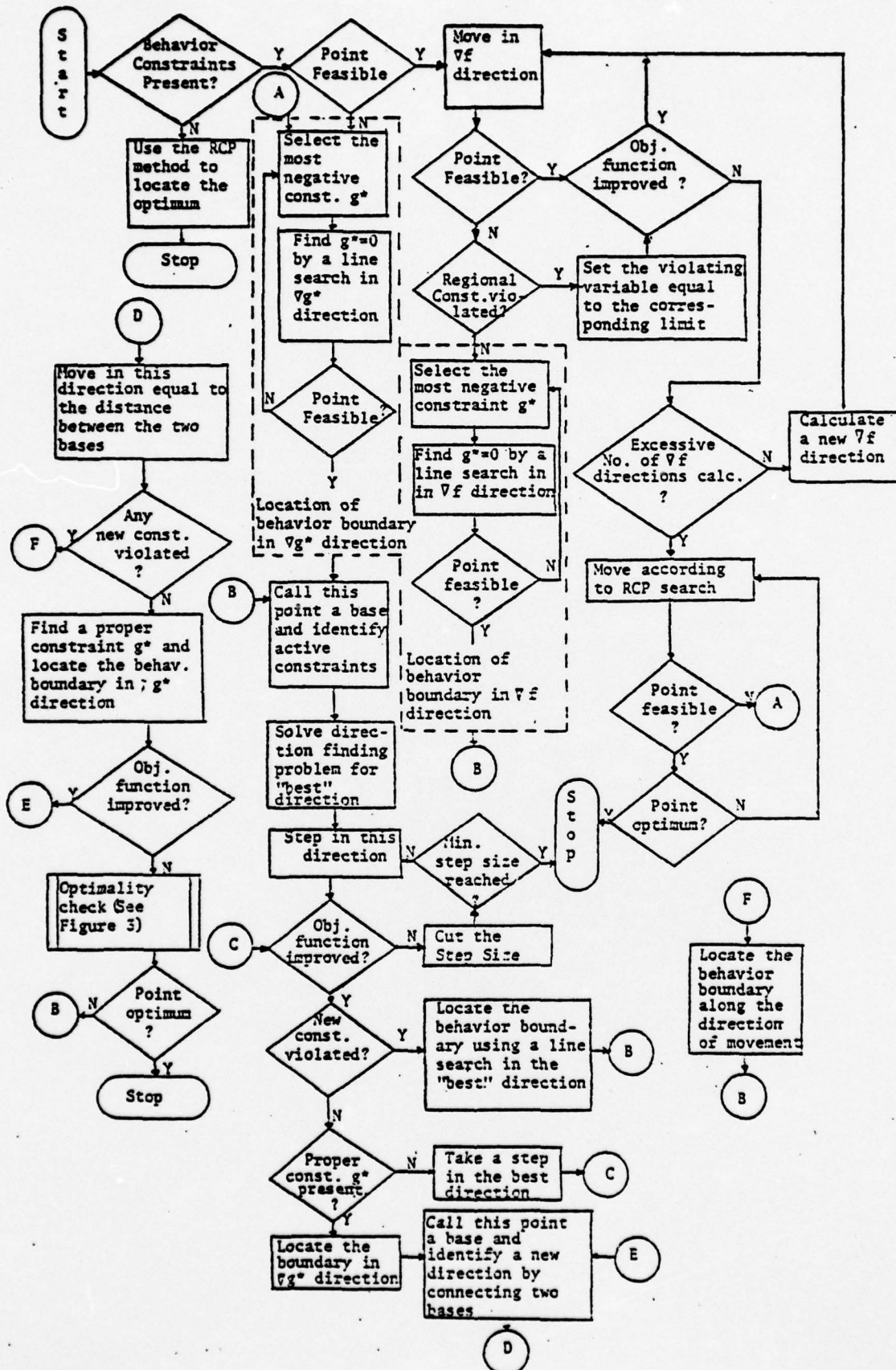


Figure 2 - Block Diagram of the General Strategy

continues, doubling the step size with each move.

Once the behavior boundary is crossed, a point on this boundary is located (point 5) using a line search in the direction of the last move.

The search is performed in the direction of movement, rather than say the direction of the gradient of the constraint function violated, since identification of the latter direction requires calculation of constraint function derivatives, while the former direction is available and thus requires no new information. The line search is used because of its simplicity.

If the search move crosses the IF boundary at a regional limit, it is possible to find the best direction to continue movement by solving Zoutendijk's direction finding problem (see section 3.2.3). Here for simplicity, however, the variables exceeding the limits are set equal to the corresponding limit and the search continued until a behavior constraint is violated. This strategy tends to deflect the direction of movement along the IF boundary.

If after a step, the point remains in the feasible region but the objective function has not improved, a new gradient direction is calculated at the last base point and the search restarted. If several direction changes fail to locate the constraint boundary, a more efficient, albeit more complex, unconstrained search method such as the modified Rotating Coordinate Pattern (RCP) search [17], is

used. This search procedure is applied here to avoid the zig-zagging problem associated with the gradient search method [12]. Thus the advantages of the gradient search method are exploited where possible, but the method is replaced by a more appropriate procedure whenever strategy dictates. If the behavior boundary is crossed in the modified RCP search, the nearby boundary may be located by any convenient method such as that already described.

The major contribution of this thesis is the procedure for movement along the behavior boundary. It is this movement which causes the difficulty associated with the solution of constrained nonlinear problems. The method used for locating the boundary, such as the gradient search or the RCP search, is of secondary importance. Since the bulk of the search is associated with movement along the boundary, the choice of the initial boundary locating procedure will not substantially effect overall performance. Thus, the procedures used for this purpose are not of great importance and need not be described in detail here. The interested reader is referred to references [12, 17] for a detailed description of these methods.

If the starting point is infeasible, the behavior boundary is located by first selecting the most negative constraint, that is, the constraint presenting the greatest violation. The point where this constraint vanishes is then located using a line search in the direction of the gradient of this constraint (see section 3.1.2). This direction is used here since it provides the shortest distance to the



surface where this constraint vanishes. The line search procedure used here is a modified Secant root finding procedure (see section 3.1.2).

All the constraints are then evaluated at the point where the selected constraint vanishes. If no violation exists the objective function is evaluated and the point is designated as a base point. However, if any other constraints are violated at this point, the smallest one (algebraically) is again selected and the point where it is zero is found. This process is continued until a point on the behavior boundary is located.

For problems without behavior constraints an unconstrained search method, such as the modified RC Pattern search [18], is used to locate the optimum point. This search method combines the well known RC Pattern search with Zoutendijk's feasible direction finding method (see section 3.2.3). The direction finding procedure is employed at the points of RC Pattern search failure.

### 2.3 Movement Along The Behavior Boundary

Once the point on the behavior boundary is located it is designated as a base point (point  $x^1$  in Figure 1). The best direction to move is then determined by solving the direction finding problem of Zoutendijk (see section 3.2.3) and a step taken in this direction. The objective function is then evaluated at this point. If the function has improved, all the constraints are evaluated.



If none of the constraints that were inactive at the base are violated, an appropriate constraint is selected from among the active constraints (see section 3.1.1). The behavior boundary is located by finding a point where this constraint is zero by means of a line search in the direction of the gradient of the selected constraint (point  $x^2$ ).

Upon locating the point on the boundary after the best direction move, the objective function is evaluated. If the function has improved the point is designated as a base point (point  $x^2$ ). A move is then made from the last base in the direction of improvement along a line connecting two bases a distance equal to the distance between these bases.

The boundary is then located as before (see point  $x^3$  of Figure 1) along the direction of the gradient of the appropriate constraint as evaluated at the last point where the best direction finding problem was formulated. It should be pointed out that this is an underlying feature of this algorithm, making multiple use of function evaluations in order to keep the number of new evaluations required as small as possible. Only if this direction fails to locate the boundary, are new gradient values computed.

When the point on the behavior boundary is found, it is compared to the last base point. If the function has improved, the point is designated as a new base point (points  $x^3$ ,  $x^4$ ,  $x^5$ ) and the search is continued. However, if the function has not improved the direction

is abandoned and the search is re-started from the last base point by calculating a new best direction.

After each move all the constraints are evaluated, if a new constraint is violated (point A) the point where this constraint is zero is located and a new best direction calculated. However, if no new constraint is violated, an appropriate constraint is selected from among the previously active constraints (see section 3.1.1) and the boundary located, the process is continued until convergence is achieved.

If no appropriate constraint is active the move along the previous direction is continued, since it is the best direction available. If after a step in the above direction, the objective function has increased rather than decreased the step size is reduced. The process is repeated until a better point is found or the convergence criterion is met (see section 3.3).

If after any move a constraint inactive at the last base point is violated, the behavior boundary is located by finding the point where this constraint is zero. This point is found by a line search in the direction of the last move. This direction is used to eliminate the need to calculate the gradient of the new constraint. The search is then re-started by calculating the best movement direction at this point on the boundary.

2.4 Search termination description. For the few cases where the optimum occurs away from the behavior boundary, a sufficient condition for optimality is that all components of the gradient of the objective function be essentially equal to zero. For most cases, however, where the optimum is on the behavior boundary no such simple condition exists.

The search termination procedure used here is as follows. The search using a specified basic step size is performed until no further improvement can be obtained. When such a point is found it is designated as an optimality comparison base. Now the basic step size is reduced in an effort to achieve improvement and the search continued until a new optimality comparison base is obtained.

In order to justify a further reduction in the step size an optimality check is performed whenever the step size is to be reduced. If a convergence limit is satisfied, the step size is again reduced for further improvement and the search is continued until another optimality comparison base is obtained. A secondary convergence check is then performed in order to determine whether the latest improvement due to the step reduction is less than the previous improvement thereby indicating convergence has occurred. If both convergence tests are simultaneously satisfied, or the minimum step size is reached, the search is terminated. Otherwise, the search is re-started by calculating a new best movement direction.

A block diagram of the search termination procedure is given in Figure 3.



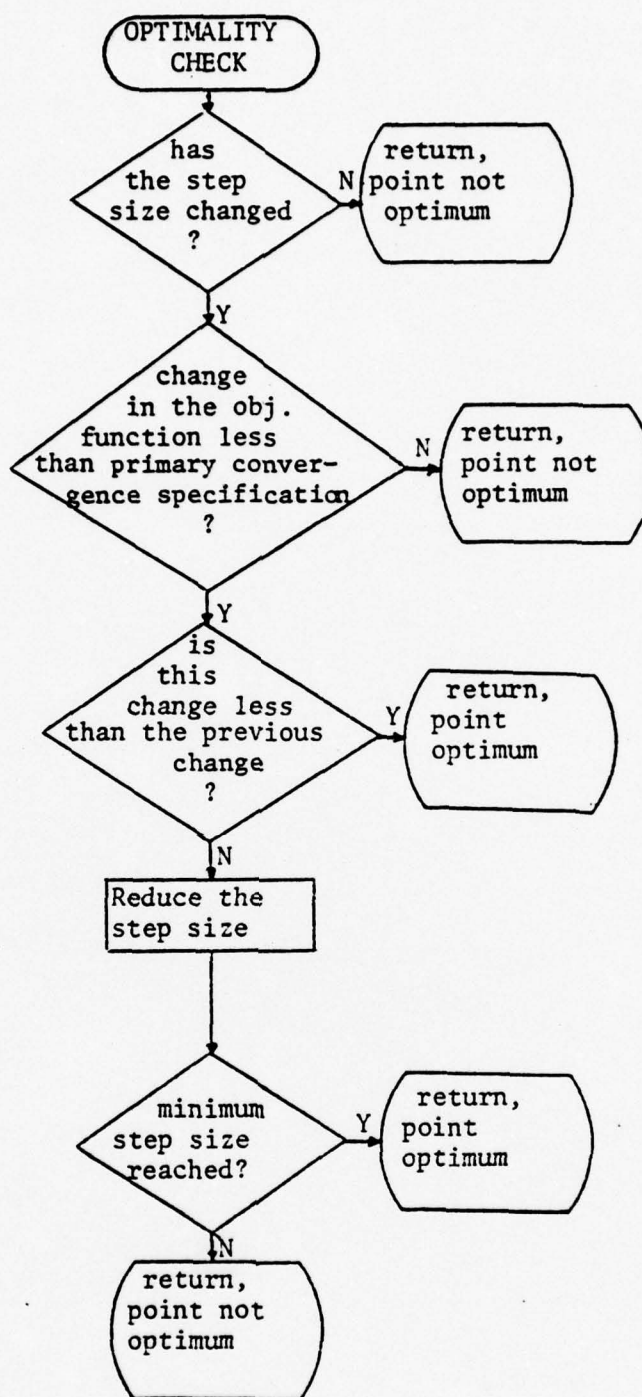


Figure 3 - Block diagram of the termination procedure

CHAPTER 3  
MATHEMATICAL DEVELOPMENT

3.1 Boundary Location

It is assumed for the purpose of devising a search strategy that the solution to the optimization problem with behavior constraints lies on the behavior boundary. The main strategy is first to locate such a boundary and then to move along this boundary. For the purpose of locating the boundary a "proper" behavior constraint is identified and method for locating the behavior boundary selected or developed.

3.1.1 Identification of "proper" constraints. All negative and small positive constraints are designated as active constraints (for definition of activity see section 3.2.3). A constraint is considered "proper" if it is necessary or desirable to locate a point where the value of this constraint is zero after making a search move in an effort to establish a new base.

Since it is necessary to eliminate any constraint violation present at a point, all the negative constraints are considered "proper".

If all active constraints are positive, a positive active constraint is considered proper if

$$-\nabla f \cdot \nabla g_j < 0 \quad (3.1)$$

This indicates that the projection of  $-\nabla f$  on  $\nabla g$  is of opposite sign to  $\nabla g$  (point 1 Figure 4) and therefore, the value of the constraint

$g_j$  will decrease as a result of a move in  $-\nabla f$  direction (minimization problem).

The best direction for improving a function is its gradient direction. However, this direction is not always feasible in constrained problems (point 1 Figure 4).

A direction is desired such that after taking a step, the objective function will improve the maximum amount possible without violating the behavior constraints. A direction along the behavior boundary often has this property. Moving along the behavior boundary, however, may not always produce the best improvement in the objective function as shown by point 2 in Figure 4. Here projection of  $-\nabla f$  on  $\nabla g_j$  has the same sign as  $\nabla g_j$ . Thus, the value of the constraint  $g_j$  will increase by moving in  $-\nabla f$  direction. A criteria is therefore needed that can indicate which positive constraint (if any) is "proper". Equation (3.1) satisfies this purpose, since if satisfied it identifies the constraints that may be violated if a move in the best direction ( $-\nabla f$ ) is made. Thus it identifies proper constraints, that is, those constraints along which it is desirable to move in order to achieve the best improvement in the objective function.

If no proper constraint can be identified, the movement along the previous direction is continued, since there is no advantage in locating and moving along the nearby boundary.

3.1.2 The boundary locating method. Call the set of proper constraints  $P_k$  where,  $k = 1, 2, \dots, K$ . If more than one "proper"

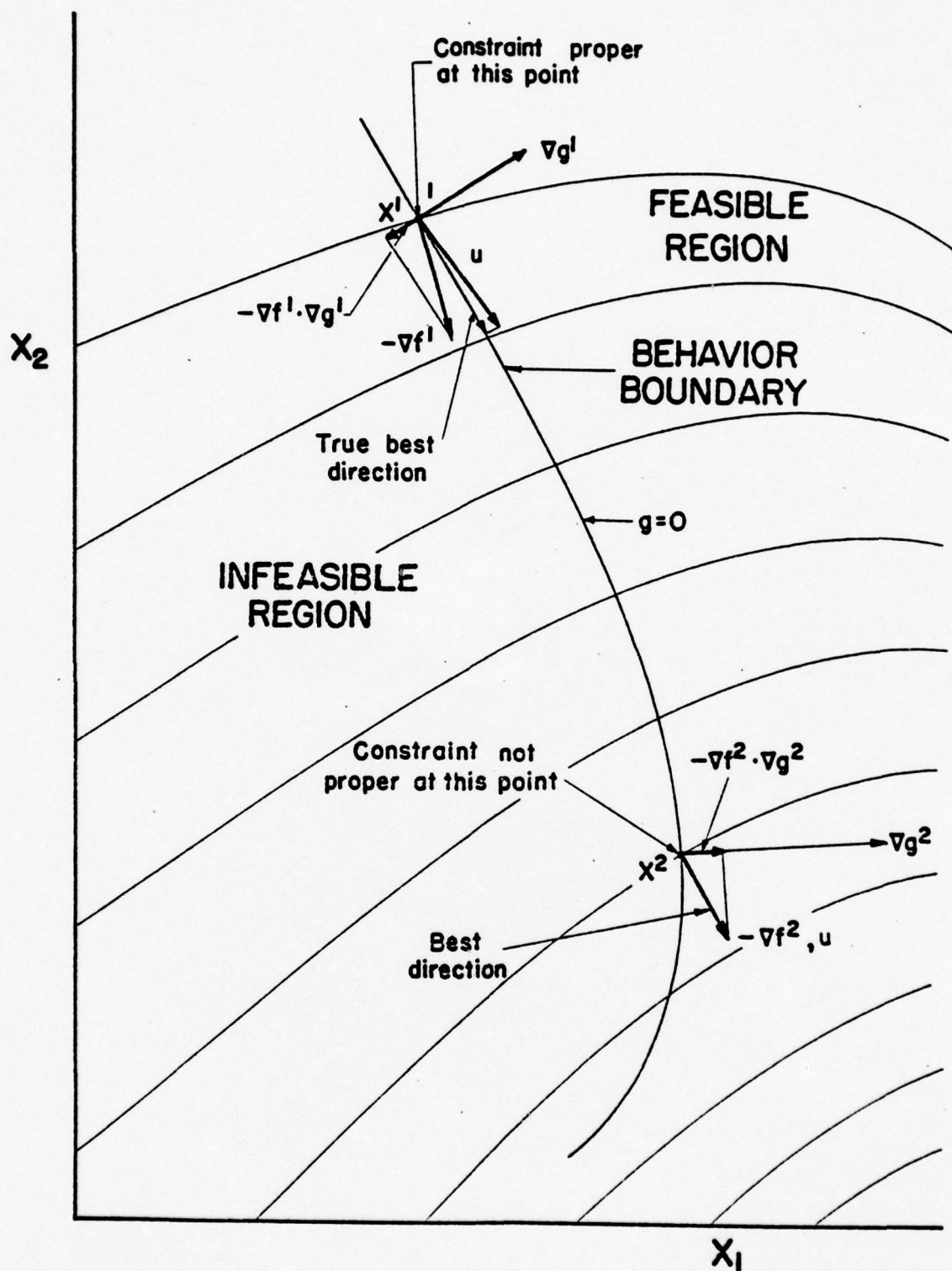


Figure 4 - Selection of a Proper Constraint



constraint is identified, that is if

$$K > 1 \quad (3.2)$$

the smallest (algebraically) is selected and called  $g^*$ . The root of  $g^*$  is then found in the direction of movement or the gradient of  $g^*$ .

The root, if it exists, of the constraint  $g^*(x)$  along a line may be found as closely as desired by means of the "secant root-finding" method [19] by iterating the equation

$$x^{s+1} = x^s - g^*(x^s)(x^s - x^{s-1}) / [g^*(x^s) - g^*(x^{s-1})] \quad s = 1, 2, \dots, N_1 \quad (3.3)$$

where  $N_1$  is the maximum number of iterations permitted, until

$$|g^*(x^{s+1})| \leq e_1 \quad (3.4)$$

is satisfied. Here  $e_1$  is an arbitrarily selected accuracy limit.

Initially  $x^s, x^{s-1}$  are two points on the line defined by

Case A: If the boundary is to be located in the direction of the last search move (see section 2.3) let the initial points on the line ( $s = 1$ ) be given by

$$x^{s-1} = x^b \quad (3.5)$$

$$x^s = x^r \quad (3.6)$$

where  $x^b$  and  $x^r$  are the end points of the last search step.

Case B: If the boundary is to be located in the gradient direction of the constraint  $g^*(x)$  (see section 2.3) let

$$x^{s-1} = x^r \quad (3.7)$$

$$x^s = x^r \pm \alpha^n \nabla g^*(x^n) / (\nabla g^*(x^n)) \quad (3.8)$$

where  $x^r$  is the point from which the boundary is to be located and  $x^n$  is the last base where a direction finding problem was formulated

(see section 3.2.3.). Here the plus and minus signs are used when  $g^*$  is negative or positive respectively. The quantity  $\alpha^n$  is the step size used at point  $x^n$ .

Case C: For the case where this procedure is used to find the behavior boundary where a starting point of the optimal search is infeasible, replace  $x^r$  by the starting point  $x^0$  and let,

$$\alpha^n = \alpha^0 \quad (3.9)$$

where  $\alpha^0$  is an arbitrarily specified initial step size, and let

$$\nabla g^*(x^n) = \nabla g^*(x^0) \quad (3.10)$$

in equations (3.7) and (3.8).

After equation (3.4) is satisfied, the remainder of constraints in the set  $P_K$  may also vanish. However, if after eliminating the the smallest violation

$$g_j(x^{s+1}) \geq -e_j \quad j = 1, 2, \dots, J \quad (3.11)$$

is not satisfied, a new  $g^*$  is selected and the procedure repeated until a point on the behavior boundary is located (equation 3.11 satisfied).

In case B, slow convergence may indicate that the gradient  $\nabla g^*(x^n)$  may no longer be applicable at point  $x^n$ . This situation is shown in Figure (5). There is no point along the gradient  $\nabla g^*(x^1)$  which falls on the boundary. A new gradient direction  $\nabla g^*(x^r)$  is therefore calculated and used in place of  $\nabla g^*(x^n)$ . If after calculating a new gradient direction the boundary still cannot be located with a reasonable number of iterations, the difficulty may be due to too large a reach step (line  $x^6 - x^r$  in Figure 5). Thus where recalculation of the

gradient fails, the step size is reduced and another effort is made to locate the boundary from a point somewhat closer to the last base.

Therefore, unless

$$s < N_1 \quad (3.12)$$

where  $N_1$  is chosen empirically, let

$$\nabla g^*(x^n) = \nabla g^*(x^r) \quad (3.13)$$

in equation (3.8) and repeat the application of equation (3.3). If equation (3.12) is again violated let

$$\Delta x^{r+1} = \Delta x^r / 2 \quad (3.14)$$

where

$$\Delta x^r = x^r - x^b \quad (3.15)$$

and  $x^b$  is the last base point. Then select the smallest proper constraint at point  $x^{r+1}$  where

$$x^{r+1} = x^b + \Delta x^{r+1} \quad (3.16)$$

(point  $x^b + \Delta x^{r+1}$  in Figure 5), replace  $x^r$  by  $x^{r+1}$  in equations (3.7) and (3.8) and repeat the iteration of equation (3.3). The process is continued until the boundary is located without violating equation (3.12) or until

$$|\Delta x^{r+1}| < \alpha^n. \quad (3.17)$$

If equation (3.17) is satisfied the attempt to locate the boundary is abandoned. The optimal search is then restarted by calculating a new starting direction (see section 3.2.3) at the last feasible point encountered.

### 3.2 Mathematical Representation of General Strategy

The general strategy of the algorithm can be represented mathematically as follows.

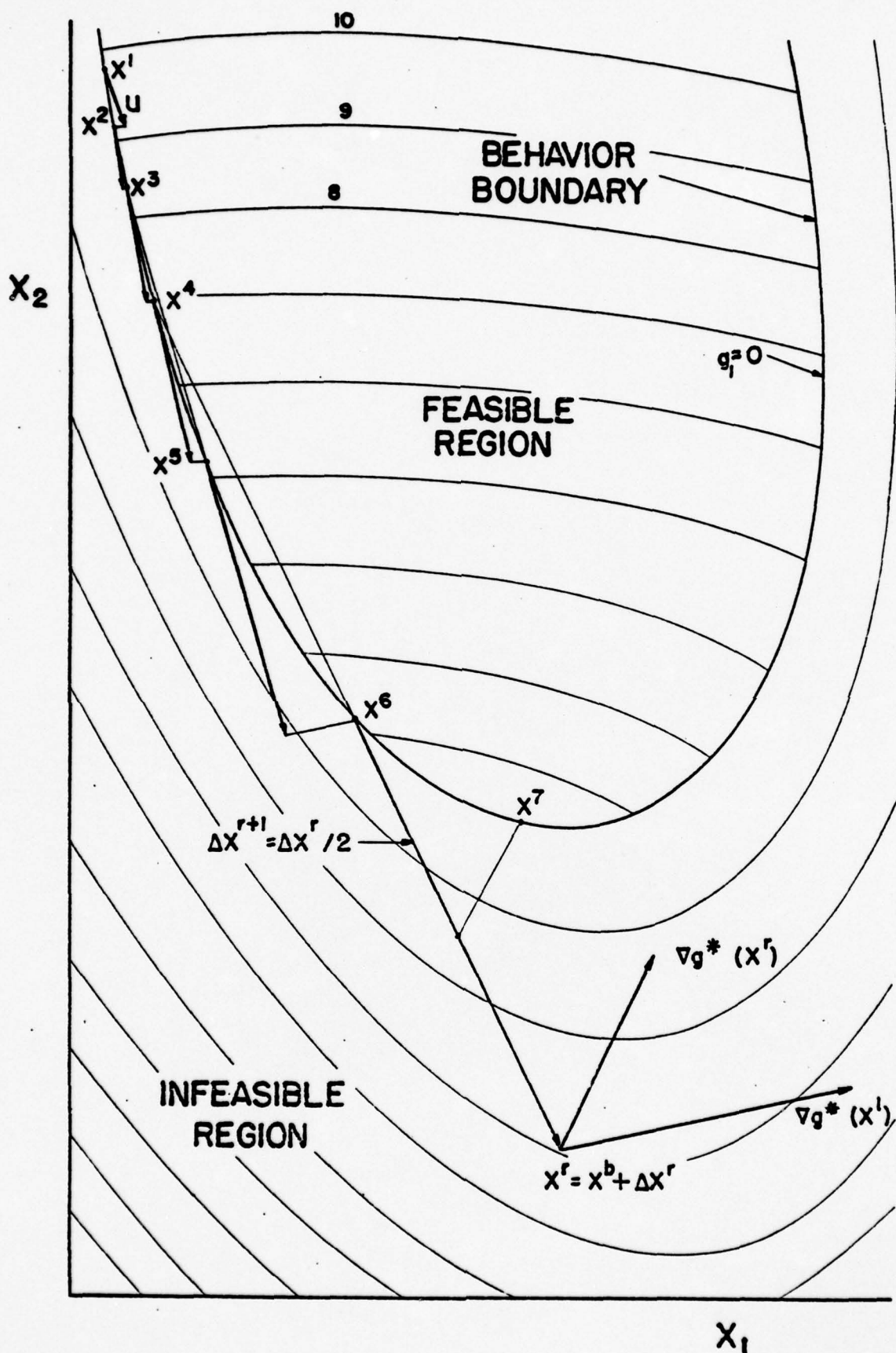


Figure 5 - The Boundary Locating Method



3.2.1 Movement to the boundary-starting point in the feasible region. A block diagram for the movement to the boundary procedure is given in Figure 6.

Given the starting point  $x_i^r$ , where initially  $r = 0$ , which satisfies regional constraints

$$x_i^L \leq x_i^r \leq x_i^U \quad i = 1, 2, \dots, I \quad (3.18)$$

and all

$$g_j(x_i^r) \geq 0 \quad j = 1, 2, \dots, J \quad (3.19)$$

the objective function  $f(x^r)$  is evaluated. This point is called a base point  $x^b$ , where initially  $b = n = 1$ , and the first comparison base  $x^n$  is defined as,

$$x^n = x^b \quad (3.20)$$

Then with

$$\alpha^r = \alpha^n \quad (3.21)$$

let

$$x^{r+1} = x^r - \alpha^r [\nabla f(x^n)] / |\nabla f(x^n)| \quad (3.22)$$

where  $\nabla$  is the gradient operator,  $|\nabla f|$  the magnitude of  $\nabla f$  and,  $\alpha^r$  is the step size at iteration  $r$ .

If any

$$\left. \begin{array}{l} x_i^{r+1} > x_i^U \\ x_i^{r+1} = x_i^U \end{array} \right\} \quad (3.23)$$

let

or if any

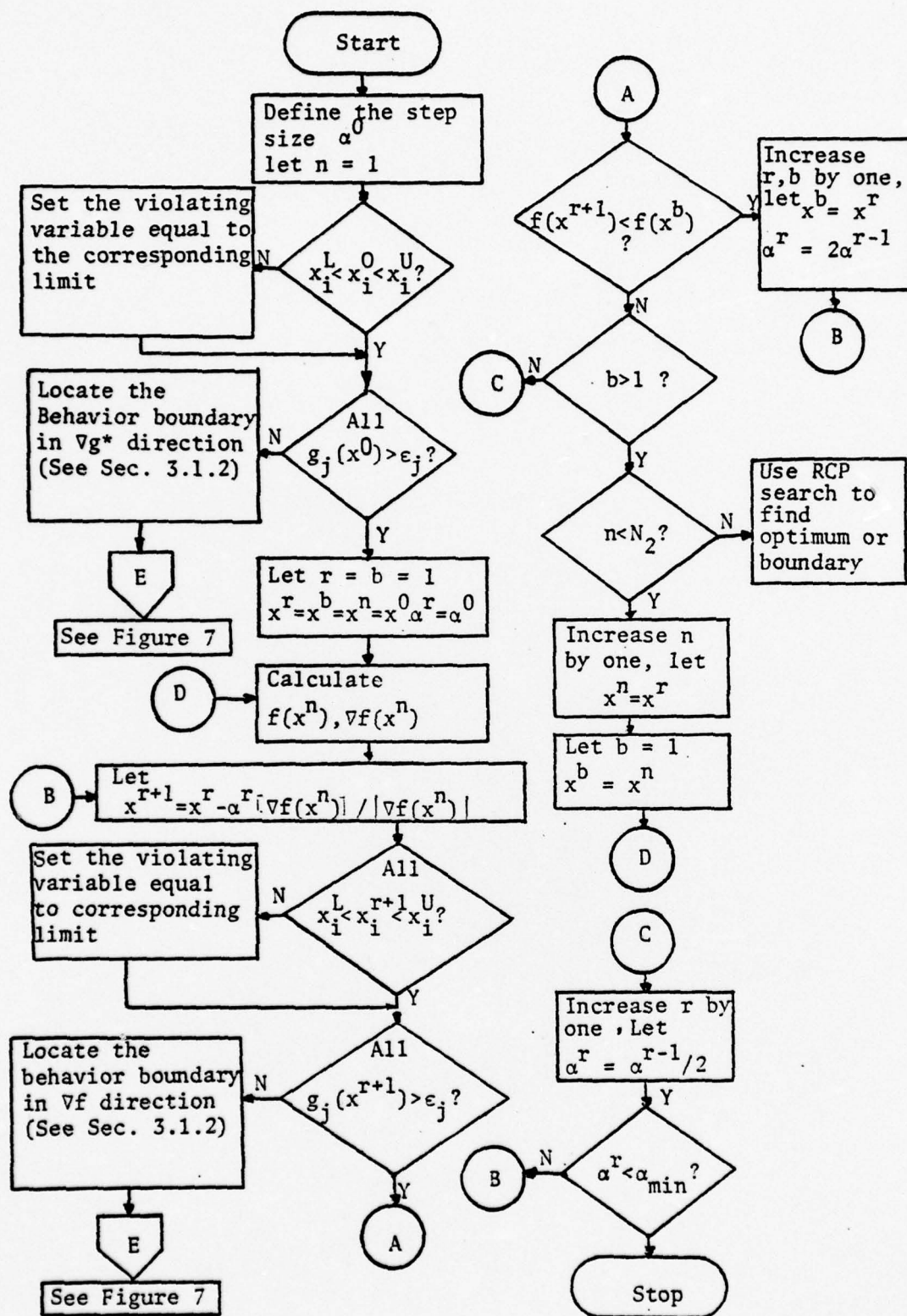


Figure 6 - Flow Chart of the Procedure for Movement to the Boundary

$$\text{let } \left. \begin{array}{l} x_i^{r+1} < x_i^L \\ x_i^{r+1} \approx x_i^L \end{array} \right\} \quad (3.24)$$

Now compute the  $g_j(x^{r+1})$ , if equations (3.19) are satisfied, evaluate  $f(x^{r+1})$ . If

$$f(x^{r+1}) < f(x^b) \quad (3.25)$$

call the point a new base point. Thus let

$$x^{b+1} = x^{r+1} \quad (3.26)$$

A new move is then made according to equation (3.22) with the step size redefined as

$$\alpha^{r+1} = 2\alpha^r \quad (3.27)$$

and application of equations (3.23-3.26) repeated. If  $b > 1$  and equation (3.25) is not satisfied increase  $n$  by one, let the next comparison base

$$x^n = x^b \quad (3.28)$$

and let

$$x^r = x^b \quad (3.29)$$

Now if

$$n < N_2 \quad (3.30)$$

where  $N_2$  is an arbitrary constant signifying the number of direction changes, a new gradient direction  $\nabla f$  is calculated. The application of equations (3.20-3.27) are then repeated until either a point in the infeasible region is found or equation (3.30) is not satisfied. If point  $x^{r+1}$  is in the infeasible region the behavior boundary is located in the direction of the last move (see section 3.1.2).

If  $n$  exceeds  $N_2$  the gradient search is abandoned and the RCP search invoked. This search method is continued in the unconstrained

region until a point in the infeasible region is found or the optimum is achieved (see section 3.3).

If equation (3.25) is not satisfied when  $b=1$ , the step size  $\alpha$  is redefined as

$$\alpha^{r+1} = \alpha^r/2 \quad (3.31)$$

and a new move is made according to equation (3.22). The application of equations (3.31) and (3.22) is repeated until equation (3.25) is satisfied or

$$\alpha^{r+1} \leq \alpha_{\min} \quad (3.32)$$

where  $\alpha_{\min}$  is a minimum step size. In the latter case the point is assumed to be optimum and the search is terminated.

3.2.2 Movement to the boundary - starting point in the infeasible region. If the starting point  $x_i^0$  is in the infeasible region or the RCP search has located a point in this region the behavior boundary is located by a search in a constraint gradient direction (see section 3.1.2).

3.2.3 Initiation of movement along the boundary. After locating a point on the behavior boundary a method is needed which can initiate the move along this boundary toward the optimum if optimality has not yet been achieved. The Feasible direction finding algorithm of Zoutendijk [20] is suitable for this purpose since, it either provides a direction along which an improved point can be found, or indicates the presence of a local optimum.



Definition: a) A direction vector  $u$  is called "feasible" if after taking a sufficiently small step along this direction no constraint is violated [20]. This will be true if

$$(u)^T \nabla g_j(x) \geq 0 \quad (3.33)$$

where  $(u)^T$  is the transpose of  $u$ , since a small step in this direction will produce no change or an increase in  $g_j(x)$ .

b) A feasible vector  $u$  is called "usable" if a move in the direction  $u$  can also provide an improvement in  $f(x)$ . This will be the case if

$$(u)^T \nabla f(x) < 0 \quad (3.34)$$

since a sufficiently small step in the  $u$  direction will produce a decrease in the value of  $f(x)$ .

c) A behavior constraint  $g_j(x)$  is considered "active" if

$$g_j(x_i) \leq \epsilon_j \quad (3.35)$$

where

$$\epsilon_j = K_j (\alpha^n / \alpha^0) \quad (3.36)$$

is an array of positive, arbitrary small numbers. These numbers may approach zero during the search, but can not be identically zero [20]. The quantity  $\alpha^0$  is the step size at the beginning of the search and  $K_j$  is a small positive constant.

d) A lower regional constraint is considered "active" if

$$x_i - x_i^L \leq \alpha^n \quad (3.37)$$

and the upper constraints active if

$$x_i^U - x_i \leq \alpha^n \quad (3.38)$$

Denote the set of all active behavior constraints by  $A_j$ . Call  $R_i^-$  and  $R_i^+$  the active lower and upper regional constraint set respectively.

The direction finding problem can be formulated in the following manner:

Given  $x$ , find  $u$  that results in the

$$\max \sigma \quad (3.39)$$

and for which

$$\sigma > 0 \quad (3.40)$$

$$(u)^T \nabla f(x) + \sigma \leq 0 \quad (3.41)$$

$$-(u)^T \nabla g_j(x) + W_j \sigma \leq 0 \quad j \in A_j \quad (3.42)$$

$$u_i \leq 0 \quad i \in R_i^- \quad (3.43)$$

$$u_i \geq 0 \quad i \in R_i^+ \quad (3.44)$$

$$|u_i| \leq 1 \quad i = 1, 2, \dots, I \quad (3.45)$$

Equations (3.45) bound the length of  $u$  to prevent the direction finding problem from producing an unbounded solution vector.

When suitable deflection parameters  $W_j$  are used, the solution of the problem provides a usable and feasible direction  $u$  since, if  $\sigma > 0$  from equations (3.41) and (3.42) equations (3.33) and (3.34) will be satisfied. It also provides the best usable direction since, if  $\sigma$  is maximized, the left hand side of equation (3.34) will be a maximum and therefore the direction found will be the best direction for decreasing  $f(x)$  [20].

It may be seen that the direction finding problem of equations (3.39 - 3.45) is a linear programming problem. Thus, any linear programming method such as the simplex procedure [21] can be used to provide the solution.

Since the objective here is to move along the IF boundary, the direction  $u$  should be as close to this boundary as possible. The work associated with locating the boundary will therefore be minimized after the move. The deflection parameters  $W_j$  here are thus set to be equal to zero. This produces a direction  $u$  that tends to be tangent to the boundary.

3.2.4 Movement along the boundary. A flow chart for the movement along the boundary procedure is given in Figure 7.

Call the point on the behavior boundary  $x^b$  and define

$$\alpha^{\ell} = \alpha^n \quad (3.46)$$

where initially  $b = \ell = 1$ ,  $x^b$  is a base point, and  $\alpha^{\ell}$  is a comparison step size. A direction  $u$  is then calculated (see section 3.2.3) and the point  $x^r$  defined as

$$x_i^r = x_i^b + \Delta x_i^r \quad (3.47)$$

where

$$\Delta x_i^r = \alpha^{\ell} u_i / |u| \quad (3.48)$$

if

$$f(x^r) < f(x^b) \quad (3.49)$$

and

$$g_j(x^r) > \epsilon_j \quad \begin{matrix} j = 1, 2, \dots, J \\ j \notin A_j \end{matrix} \quad (3.50)$$



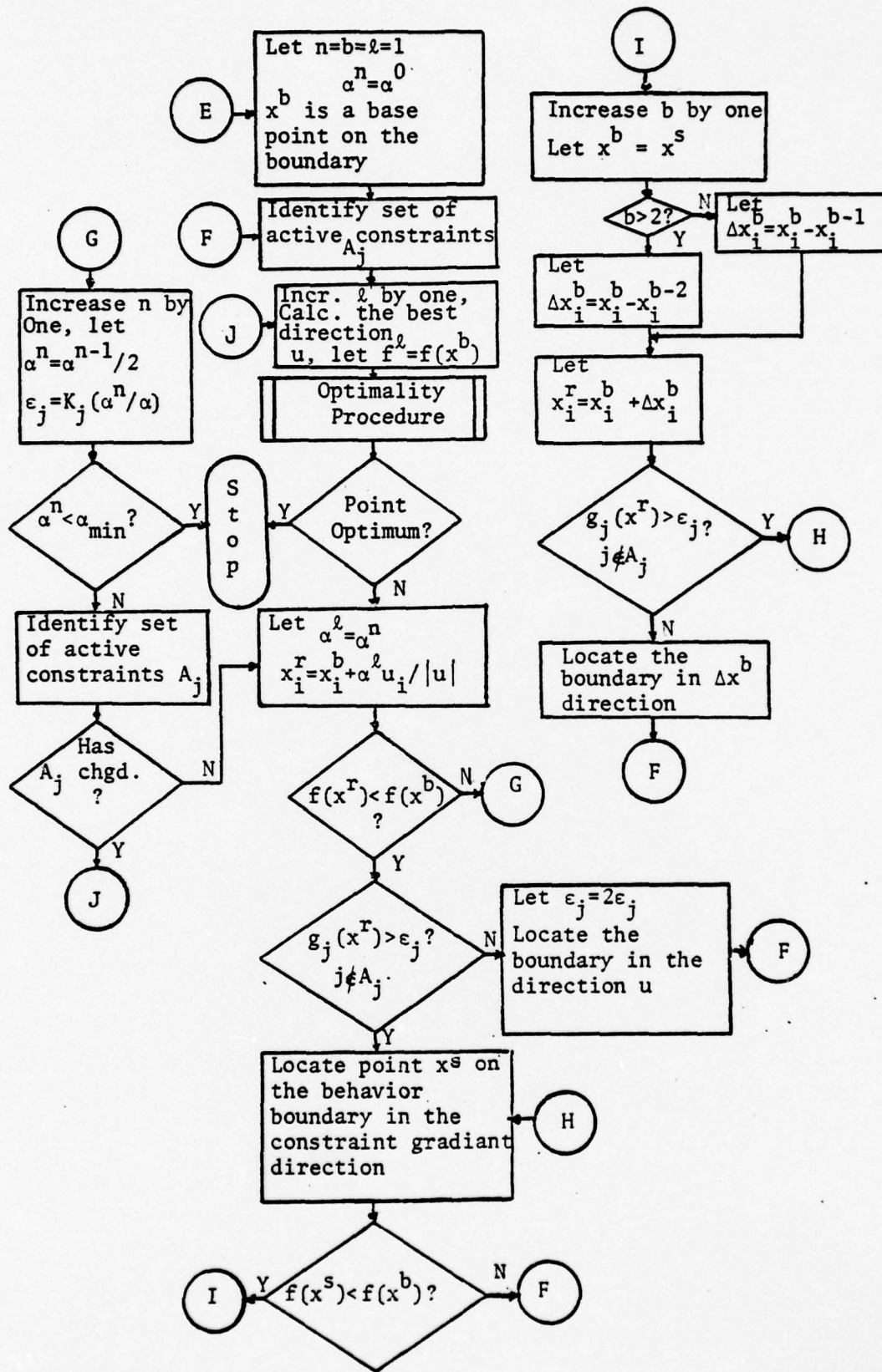


Figure 7 - Flow Chart of the Procedure for Movement along the Boundary



are satisfied, point  $x^S$  on the behavior boundary is located by a search in the constraint gradient direction and the objective function evaluated. Now, if equation (3.49) is satisfied at  $x^S$ , let

$$x^{b+1} = x^S \quad (3.51)$$

now index  $b$  and define the next step as

$$x_i^r = x_i^b + \Delta x_i^r \quad (3.52)$$

where

$$\Delta x_i^r = x_i^b - x_i^{b-2} \quad b > 2 \quad (3.53)$$

or

$$\Delta x_i^r = x_i^b - x_i^{b-1} \quad b = 2 \quad (3.54)$$

The constraints are now evaluated. If equation (3.50) is satisfied, the behavior boundary is located in the constraint gradient direction and the application of equations (3.51 - 3.54) repeated.

If when  $b=1$ , equation (3.50) is not satisfied, that is, if new constraints have become active, the value activity limit  $\epsilon_j$  is doubled for all constraints in set  $A_j$  not satisfying equation (3.50), since its previously assigned value was not sufficient to properly define activity. The boundary is then located in the direction  $u$  and the application of equations (3.47 - 3.50) repeated.

If equation (3.50) is not satisfied when  $b > 2$  the boundary is located in the direction of the last move  $\Delta x^r$ . Then a new set of active constraints is defined and the search re-started from the last base point (see section 3.2.3).

In application of equations (3.49 - 3.54) if equation (3.50) is satisfied, but equation (3.49) is not satisfied, this indicates that the last search move direction was unproductive, therefore the last direction of movement is abandoned and the search is re-started from the last base point  $x^b$  by calculating a new direction  $u$ , and setting  $b=1$ .

After employing equations (3.47) and (3.48), if equation (3.49) is not satisfied, this indicates that the step size is too large, therefore let

$$\alpha^{n+1} = \alpha^n/2 \quad (3.55)$$

$$\alpha^{l+1} = \alpha^{n+1} \quad (3.56)$$

Now, since new activity limits are defined [see equation (3.36)] the active constraints are again determined, if the set  $A_j$  has changed a new direction  $u$  is calculated, otherwise the previous direction is used and application of equations (3.47 - 3.49) repeated using the new step size. This procedure is continued until equation (3.49) is satisfied or convergence is achieved.

Application of equations (3.47 - 3.56) is invoked when applicable, as explained above, until the convergence or optimality criterion are met (see section 3.3).

### 3.3 Search Termination

A flow chart for the search termination procedure is given in Figure 8.

The question of optimality is considered at all points where the direction finding problem is formulated. For the few cases where a local optimum occurs away from the behavior boundary that is where all

$$g_j(x) > \epsilon_j \quad (3.57)$$

a sufficient condition for optimality is

$$|\nabla f| \leq e_2 \quad (3.58)$$

where  $e_2$  is an arbitrary small number.

For most cases, however, where optimum is constrained, the solution to Zoutendijk's direction finding problem [20] provides a test for optimality. A null solution vector  $u$  indicates a local optimum where all  $\epsilon_j = 0$ . However, where some  $\epsilon_j \neq 0$  and the active constraints are also not zero, the point may be merely near, rather than at the optimum, since in this type of problems the optimum point is usually on the behavior boundary. Therefore, when  $u = 0$  attempts are made to re-start the search and the optimality procedure is invoked only when a non-zero direction vector  $u$  is obtained. In order to re-start the search the step size is redefined as

$$\alpha^{n+1} = \alpha^n / 2 \quad (3.59)$$

and therefore the activity limits  $\epsilon_j$  are redefined according to equation (3.36). A new direction  $u$  is then calculated if  $A_j$  has changed. This procedure is repeated until a non-zero direction is found or the minimum step size is encountered, that is

$$\alpha^n \leq \alpha_{\min} \quad (3.60)$$

in which case the search is terminated and the point is assumed to be



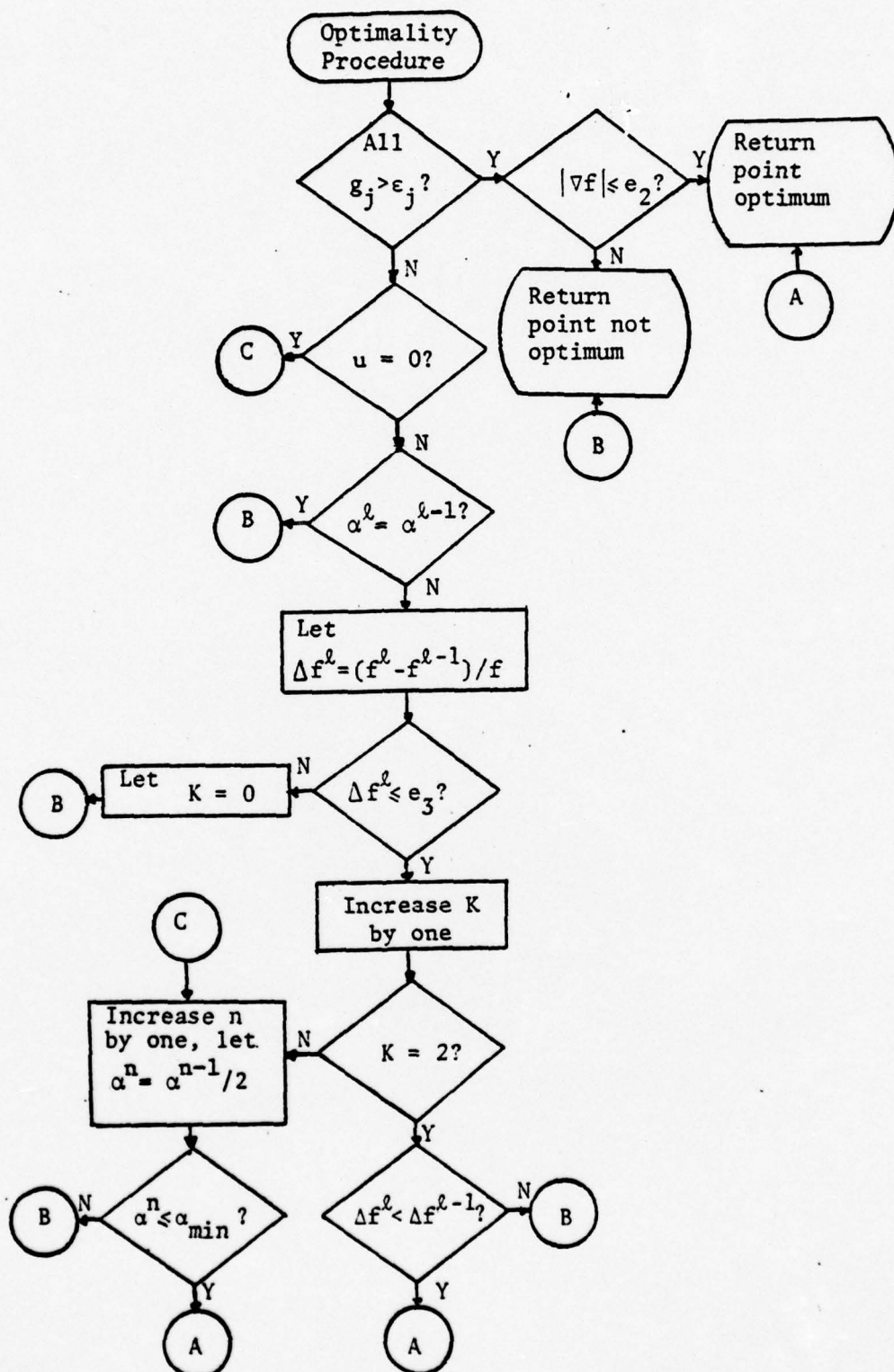


Figure 8 - Flow Chart of the Termination Procedure



an optimum.

For the cases where  $u \neq 0$ , increase  $\ell$  by one and let

$$\alpha^\ell = \alpha^n \quad (3.61)$$

$$f^\ell = f(x^b) \quad (3.62)$$

where  $f^\ell$  is a comparison value with initially  $\ell = 0$ , and  $f^0 = C_1$ , where  $C_1$  is an arbitrary large number. Now if

$$\alpha^\ell = \alpha^{\ell-1} \quad (3.63)$$

no optimality check is made since  $\ell$  has increased because the search was re-started due to the fact that the previous movement direction was unproductive. However, if the step size has changed, this indicates that the maximum improvement in the function has been achieved using the previous step size and the step size must be reduced for additional improvement. A convergence check is now made in order to determine if a search using the new step size is justified. Thus, where equation (3.63) is not satisfied, define

$$\Delta f^\ell = |(f^\ell - f^{\ell-1}) / f^\ell|. \quad (3.64)$$

Unless

$$\Delta f^\ell < e_3 \quad (3.65)$$

where  $e_3$  is the primary convergence criteria, the search is continued.

A secondary convergence check is initiated whenever the primary convergence criteria is met, [equation (3.65) satisfied] in order to confirm optimality. For this purpose the step size  $\alpha$  is reduced according to equation (3.59) and the search is re-started. When further movement with the new step size terminates the primary convergence check is invoked. Therefore, whenever equation (3.65) is not

satisfied at point  $x^b$ , let

$$K = 0 \quad (3.66)$$

and where equation (3.65) is satisfied index  $K$  and let

$$\alpha^{n+1} = \alpha^n/2 \quad (3.67)$$

$$\alpha^{l+1} = \alpha^{n+1} \quad (3.68)$$

If equation (3.60) is satisfied, the point is assumed to be a local optimum and the search is terminated. Otherwise a new direction  $u$  is computed and the search continued. When the primary convergence check is satisfied in two consecutive tries, that is if

$$K = 2 \quad (3.69)$$

the secondary convergence check is invoked. Thus if

$$\Delta f^l < \Delta f^{l-1} \quad (3.70)$$

the search is terminated. Otherwise a new direction  $u$  is computed,  $K$  is set equal to 1 and the search continued. When equation (3.70) is satisfied, the change in the value of the objective function ( $\Delta f$ ) has decreased from the previous convergence check, even though a reduced step size was used, the point is thus assumed to be optimum and the search is terminated.

## CHAPTER 4

### DESIGN EXAMPLE

#### 4.1 Problem Statement

Consider the minimum weight design of submersible, circular, cylindrical shells reinforced by equally spaced "T" type frames. The design variables with respect to which the optimization is to be carried out are: Plate thickness, frame web and frame flange thickness, frame flange width, web height, and frame spacing. The objective function to be minimized is the ratio of shell weight to the weight of fluid displaced. All the standard design equations used in submersible shell design practice are to be satisfied. All variables will be treated as continuous. The fixed design parameters are: The operating depth, shell diameter, shell segment length, shell eccentricity, construction material properties, factors of safety to be used in design, maximum and minimum values permitted for the design variables, and, when required, a maximum (when external frames are used) or minimum (when internal frames are used) frame diameter.

This problem is selected here since it is a difficult and computationally demanding engineering problem which the relatively reliable optimization code, DSDA and the popular SUMT procedure, could not solve [17].

In a previous study [22] it has been shown that the merit surface in this problem is fairly flat, therefore a wide range of variables



with similar objective function values may be generated during the search. This study also demonstrates that movement along the behavior boundary is very difficult in this problem.

A modified version of this problem with only four variables was treated in Reference [22], using the DSDA procedure. The formulation of the more difficult six variable problem presented here is similar to that used in Reference [22].

Only CADOP3 [23], a modified version of CADOP2 code, [16] reached an optimal solution to this problem. This code is three times faster than CADOP2 code in problems with behavior constraints. However, due to the difficulties involved in moving along the behavior boundary, the execution time required by CADOP3 to achieve the optimum is quite long (see section 4.3). The problem, therefore, was treated using the BT algorithm in order to demonstrate its superior ability in moving along a difficult behavior boundary.

## 4.2 Problem Formulation

4.2.1 Objective function. For cylindrical vessels with periodic "T" type reinforcing frames the objective function may be written as

$$f(x) = \begin{cases} W/\gamma_w V_D & \text{internal frames} \\ W/[\gamma_w(V_D + V_w + V_f)] & \text{external frames} \end{cases} \quad (4.1)$$

where  $W$  is the weight of the hull segment, given by

$$W = \gamma_s (V_s + V_w + V_f) \quad (4.2)$$



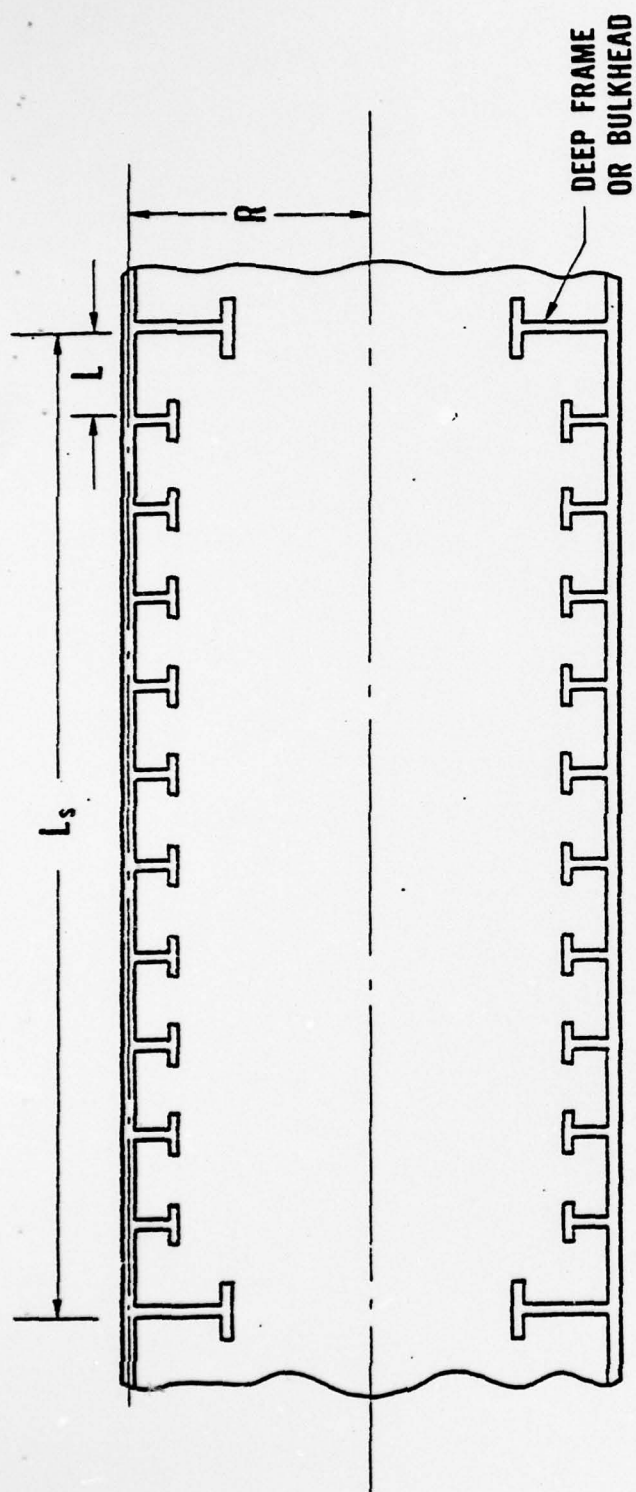
The  $\gamma_s$  and  $\gamma_w$  are the specific weight of the material and immersion fluid, respectively.  $V_s$ ,  $V_w$ ,  $V_f$  are the volume of the plating, frame webs, and frame flanges, respectively, and  $V_D$  is the displacement volume of the cylinder enclosed by the plating envelope. The variables  $x_1, x_2, \dots, x_6$ , which in turn represent the quantities  $t, b, b', w, L',$  and  $h$ , respectively, are defined in Figure 9. The objective function  $f(x)$ , therefore represents the ratio of the shell weight to the weight of the fluid displaced for the shell segment of length  $L_s$ . The weight of the bulkheads is omitted.

4.2.2 Constraint equations. The constraint equations  $g_j(x)$  are divided into two groups: a) Behavior constraints which control the failure modes or impose limitations on the space relationships among the variables, and b) regional constraints which specify ranges of the variables. The basic behavior constraint equations are formulated using a modified version of the design equations given in References [24] and [25].

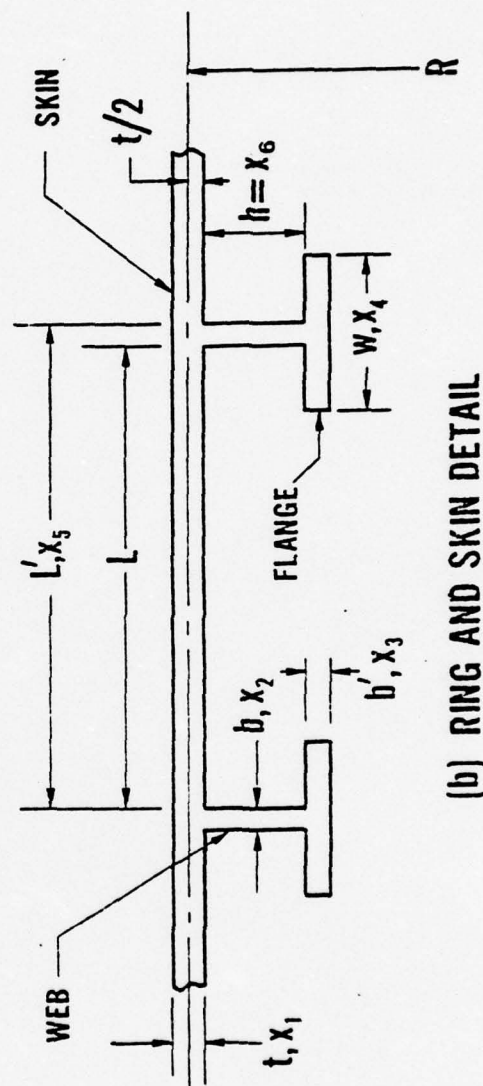
The general instability constraint is given by

$$g_1 = (p_{cg}^* - S_1 p) / p_{cg}^* \geq 0 \quad (4.3)$$

where  $p$  is the applied hydrostatic pressure;  $p_{cg}^*$  is the minimum of the collapse pressure  $p_{cg}(n,m)$  due to general instability [26], and  $S_1$  is the factor of safety for this failure mode. The collapse pressure is given by



(a) SHELL SEGMENT CROSS-SECTION



(b) RING AND SKIN DETAIL

Figure 9 - Typical Shell Cross Section

$$p_{cg}(n,m) = [Dm^2(1 + \beta^2)^2 + \frac{\beta^2 m^2}{L'} (GJ_f + EI_f \beta^2) + \frac{12DZ^2}{\pi^4 m^2} \frac{(1 + F\Lambda_f)}{\Lambda}] \frac{\pi^2}{L_s^2 R(1/2 + \beta^2)} \quad (4.4)$$

where  $p_{cg}(n,m)$  is the buckling pressure for a specified  $n$  and  $m$  and

$$\begin{aligned} \Lambda_f &= 1 + 2n^2 \bar{d} (1 - \beta^2 \mu) + n^4 \bar{d}^2 (1 + \beta^2)^2 \\ \Lambda &= (1 + \beta^2)^2 + 2\beta^2 F (1 + \mu) + \beta^4 F (1 - \mu^2) \\ Z^2 &= L_s (1 - \mu^2) / R^2 t^2 \end{aligned} \quad (4.5)$$

$$\beta = nL_s / m\pi R$$

$$F = (b_w + bh) / tL'$$

$$D = Et^3 / 12 (1 - \mu^2) \quad (4.6)$$

$$\bar{d} = d / R$$

where  $d$  is the (algebraic) distance to the neutral axis of the frame from the midplane of the hull plating, taken as positive when it is outward from the central axis of the hull [25]. The quantities  $GJ_f$  and  $EI_f$  are the torsional and bending stiffness of the frame, respectively. Symbols representing hull and frame dimensions are defined in Figure 9. The quantities  $G$ ,  $E$ , and  $\mu$  are the shear modulus  $G = E / 2(1 + \mu)$ , tensile modulus, and poisson's ratio, respectively.

Buckling of the shell between frames is controlled by the constraint

$$g_2 = (p_{cs}^* - S_2 p) / p_{cs}^* \geq 0 \quad (4.7)$$

where

$$p_{CS}(n,m) = (\pi^2/L^2 R) [Dm^2(1 + \beta^2)^2 + 1/\Lambda(12DZ^2/\pi^2 m^2)]1/(1/2 + \beta^2) \quad (4.8)$$

For a given set of design parameters and pressures the buckling pressure functions  $p_{CG}(n,m)$  and  $p_{CS}(n,m)$  depend on the two discrete independent variables, the axial and circumferential wave number  $m$  and  $n$  respectively. To obtain the critical buckling pressure one must find the minimum of  $p_{CG}(n,m)$  and  $p_{CS}(n,m)$  with respect to  $n = 0, 1, 2, \dots$  and  $m = 1, 2, \dots$ . For this purpose the procedure of Reference [26] is used here.

The necessity to avoid plating yield produces the constraint

$$g_3 = (\sigma_{pa} - \sigma_p) / \sigma_{pa} \geq 0 \quad (4.9)$$

where  $\sigma_{pa}$  is the allowable plating stress and

$$\sigma_p = (\sigma_r^2 + \sigma_\phi^2 - \sigma_r \sigma_\phi)^{1/2} \quad (4.10)$$

The quantities  $\sigma_r$  and  $\sigma_\phi$  are found from

$$\sigma_\phi = -pR/t[1 + \Gamma(H_M + \mu H_E)] \quad (4.11)$$

$$\sigma_r = -pR/2t[1 + 2\Gamma H_E] \quad (4.12)$$

The terms  $-pR/t$  and  $-pR/2t$  are the hoop and axial stresses, respectively;  $\Gamma$  is a frame deflection parameter, and  $H_M$  and  $H_E$  are the functions that define the bending effect on the shell due to local frame reinforcing [24]. Equations for  $H_M$  and  $H_E$  are given in Reference [24].

The constraint against the frame yielding failure mode is given by

$$g_4 = (\sigma_{fa} - \sigma_T) / \sigma_{fa} \geq 0 \quad (4.13)$$



where  $\sigma_{fa}$  is the allowable frame stress and  $\sigma_T$  the maximum frame stress. The quantity  $\sigma_T$  is given by

$$\sigma_T = \sigma_b + \sigma_c \quad (4.14)$$

with the compressive hoop stress  $\sigma_c$  given by

$$\sigma_c = Q_p pR / (A + bt) \quad (4.15)$$

Here  $A$  is the cross-sectional area of the frame and  $Q_p$  is the total radial load per inch of circumference.  $Q_p$  is given by equation (23) of Reference [24]. The frame bending stress  $\sigma_b$  results from slight out-of-roundness of the hull. It is calculated using

$$\sigma_b = [Ece (n^2 - 1) / R^2] [p / (p_{cs} - p)] \quad (4.16)$$

where  $c$  is the distance from the midplane of the shell to the surface of the frame,  $e$  is the eccentricity from the true circle radius, and  $n$  the wave number that minimizes  $p_{cg}$ .

It should be noted that  $\sigma_b$  is discontinuous at points near  $p = p_{cg}$  and is discontinuous with respect to  $n$ , since  $n$  is an integer.

Flange buckling is controlled by letting

$$g_5 = \sigma_b - [.5\pi^2 E / 12 (1 - \nu^2)] [x_3 / (x_4 - x_2)]^2 \geq 0 \quad (4.17)$$

Two geometric constraint equations can be used. A maximum flange thickness is specified to prevent the flange from becoming excessively thick. It is desirable to specify a maximum flange thickness as a fraction of the plating thickness. Thus, the constraint

$$g_6 = (C_2 t - b') / C_2 t \geq 0 \quad (4.18)$$

is used, where  $C_2$  is the maximum flange to plating thickness ratio.

The constant  $C_2$  is made arbitrarily large if the designer does not wish to apply this constraint. Minimum flange width is controlled by the inequality

$$g_7 = (w - C_3 h) / w \geq 0 \quad (4.19)$$

to insure that the flange width is sufficient so that the design rule for the control of the web cribbing is not invalidated,  $C_3$  is an arbitrary constant controlling the minimum ratio of flange width to web height.

It is desirable to limit the minimum or maximum (depending on whether internal or external frames are used) radius of the frame because of space consideration. One can then use the constraint

$$g_8 = (R + h + b' + t/2 - R_{\min}) / R_{\min} \geq 0 \quad (4.20)$$

where  $R_{\min}$  is the minimum specified radius for internal frames or

$$g_8 = (R_{\max} - R - t/2 - h - b') / R_{\max} \geq 0 \quad (4.21)$$

for external frames where  $R_{\max}$  is the maximum specified radius.

To insure against web buckling the following design constraint is invoked.

$$g_9 = \sigma_b - [4\pi^2 E / 12 (1 - \nu^2)] (x_2 / x_6)^2 \geq 0 \quad (4.22)$$

Side constraints of the form

$$\left. \begin{aligned} (x_i^U - x_i) / x_i^U &\geq 0 \\ (x_i - x_i^L) / x_i &\geq 0 \end{aligned} \right\} \quad (4.23)$$

are used to limit the range of the variables  $x_i$  for manufacturing, space, or other practical reasons. The flange width clearly cannot

exceed the frame spacing, imposing an upper limit on  $x_4$ . Sometimes  $x_4$  is limited by design consideration, thus if  $x_4^{U'}$  is the designer specified maximum

$$x_4^U = \begin{cases} x_4^{U'} & , & x_4^{U'} \leq x_5 = L' \\ x_5 & , & x_4^{U'} > x_5 \end{cases} \quad (4.24)$$

The formulation of the example treated here is now complete, but other forms of constraints and objective functions, which do not arise in this example are clearly possible.

### 4.3 Discussion of Results

4.3.1 Code description. A FORTRAN IV code called CADOP4 based on this algorithm was developed and used in this study. The code is operational with IBM FORTRAN levels G and H and the UNIVAC TDOS systems. The user is required to supply the objective and constraint functions, the initial values of the variables, and side constraint values.

The initial step size is internally generated so that at the starting point a step of size  $\alpha^0$  in the  $\nabla f$  direction produces a one percent change in the value of the objective function. This step is constrained so that  $\alpha^0 > .01$ . The minimum step size is defined as  $\alpha_{\min} = \alpha^0 / 1000$ . The program uses  $e_1 = 10^{-5}$ ,  $e_2 = e_3 = 10^{-6}$ ,  $N_1 = 6$ ,  $N_2 = 10$ ,  $C_1 = 10^5$  and the activity limit constant is initially specified as  $K_j = 0.01$  for all constraints.



Nondimensional constraint equations of the form

$$g_j(x_i) = (U_k - B_k) / U_k \geq 0 \quad \text{when } U_k \neq 0 \text{ and } B_k \neq 0$$

or

$$g_j(x_i) = (B_k - L_k) / L_k \geq 0 \quad \text{when } L_k \neq 0 \text{ and } B_k \neq 0$$

(4.25)

are used. Otherwise, a dimensional form of equations is used.

A constraint given as  $0 \leq b(x_i) \leq A$  would be written as two constraint equations. For example, one could be of the form of the first of equations (4.25) where  $B_1 = b(x_i)$  and  $U_1 = A$ . The second would be of the form  $g_2 = -b(x_i)$  since  $L_k = 0$ .

4.3.2 Code application. The above problem was treated using CADOP3 and CADOP4 codes. Except that the initial step size is specified for this problem as  $\alpha = 4/R$ , where  $R$  is the radius of the shell. The minimum step size is defined as  $\alpha_{\min} = \alpha^0/200$ . Runs were made on an IBM 370 model 168 using FORTRAN level G. The same starting points were used in these runs. The execution time in seconds along with other necessary information were printed at each base point in order to closely track the synthesis path of each procedure.

Tables 1 and 2 present the results obtained from CADOP3 and CADOP4 codes, respectively. A total of 72810 function evaluations were performed using CADOP3 code prior to termination. Due to the great execution time required by CADOP3 for this problem, the run was terminated prior to reaching the optimum. The execution time for this run was 56.2 seconds. CADOP4 code required only about 4000 function evaluations with 4.8 seconds execution time to reach a similar



level of convergence.

The constraint presenting the web buckling ( $g_9$ ) was active from near the beginning of the search, while the plate yielding ( $g_3$ ) became active after a relatively short time and remained active through the rest of the search. The general buckling constraint was also active at the latter part of the search. Thus, the optimal design is constrained by general instability, local web buckling and plating yield.

The CADOP3 code came within 1% of the optimum point after 23 seconds and approximately 43000 function evaluations, while CADOP4 required only 1.4 seconds and about 1000 function evaluations to reach this level of convergence. It should be pointed out that for most practical engineering purposes, a 1% level of accuracy is quite acceptable. It is the refining process that is responsible for the greatest portion of the total execution time.

It must be pointed out that due to the presence of intermediate print statements, the execution time required for solution without these statements is appreciably less than the above mentioned time. A run made without any intermediate print statements using CADOP4 code terminated after 2.1 seconds at the optimum point while the original run required 8.7 seconds.

Comparison of the above results demonstrate the apparent superiority of the Boundary Tracking algorithm to the DSFD procedure with respect to speed. This is the result of great reduction in the number

TABLE 1

SYNTHESIS PATH FOR THE SHELL DESIGN PROBLEM USING DSFD METHOD

No. of Bases	Obj. Function Value	x <sub>1</sub>	x <sub>2</sub>	x <sub>3</sub>	x <sub>4</sub>	x <sub>5</sub>	x <sub>6</sub>	No. of Obj Function Evaluations	No. of Constraint Function Evaluations	Constraints Active	CPU Time in Sec.
0	.191149	1.	.5	.5	10	10	20	3	22		.02
50	.131655	.91745	.39056	.21840	6.5253	12.9584	19.83179	1510	3209	3, 9	2.13
100	.1128944	1.19171	.35006	.13070	4.20835	27.60905	16.13659	2657	6332	3	4.21
150	.10910318	1.19397	.29135	.11307	3.2443	24.03268	13.11856	4044	9974	3	6.52
200	.108462	1.19684	.28109	.10376	2.92241	23.7068	12.60682	6782	14494	3	9.96
250	.1081338	1.1984	.27466	.10326	2.6263	23.3650	12.27031	8519	19026	3	13.37
300	.107774	1.19696	.2675	.10326	2.26339	22.437	11.887	10529	23145	3	16.67
350	.107417	1.20908	.25968	.10326	1.8243	23.6244	11.48603	12621	27486	3	20.29
400	.107051*	1.20184	.25190	.10326	1.44585	21.4827	11.0595	14621	32447	3	26.99
450	.106670	1.16294	.22833	.20389	1.02888	16.8998	10.1515	15925	35804	3, 9	31.79
500	.106545	1.1822	.22409	.25339	1.03081	16.62096	9.9441	17511	39112	3	37.51
550	.106497	1.18498	.21779	.29590	1.00365	16.785	9.7805	19730	43882	1, 3, 9	46.46
600	.106483	1.18528	.21826	.34346	.93264	16.7932	9.70967	21578	47987	1, 3, 9	52.5
623	.106477**	1.18425	.21752	.35553	.89695	16.57193	9.67398	22580	50230	1, 3, 9	56.21

\*Converged within 1% of the optimum point after approximately 375 bases.

\*\*Within .2% of the optimum point.

TABLE 2  
SYNTHESIS PATH FOR THE SHELL DESIGN PROBLEM USING THE BOUNDARY TRACKING METHOD

No. of Bases	Obj. Function Value	x <sub>1</sub>	x <sub>2</sub>	x <sub>3</sub>	x <sub>4</sub>	x <sub>5</sub>	x <sub>6</sub>	No. of Obj Function Evaluations	No. of Constraint Function Evaluations	Constraints Active	CPU Time in Sec.
Starting Point	.191149	1.0	.5	.5	10.0	10.0	20.0	1	10		
1	.146414	.95870	.37494	.37567	9.93493	11.918	19.93510	19	95	9	.11
10	.118556	1.3393	.37116	.27278	8.52995	56.78	18.52975	54	401	2, 9	.52
20	.11011	1.26089	.26746	.12878	2.20746	30.388	12.20792	81	664	9	.98
30	.10726*	1.20859	.25749	.10027	1.45954	23.173	11.3766	134	1085	3	1.63
40	.106886	1.17902	.24437	.10019	.74477	17.08	10.6618	192	1475	3	2.29
50	.106721	1.18417	.23362	.38917	.67781	17.49	10.0889	242	1822	3	2.98
60	.106652	1.18309	.22614	.471329	.75997	17.08	9.7476	316	2288	3	3.89
70	.106596	1.1837	.21881	.55404	.8405	16.99	9.4114	390	2766	3	4.81
80	.106535	1.1777	.21182	.57461	.85095	15.7	9.0787	456	3204	3	5.61
90	.106400	1.18178	.20257	.94152	.62714	15.868	8.6507	514	3603	1, 3	6.37
100	.106286	1.18286	.19107	1.0497	.60277	15.572	.503	614	4318	1, 3, 9	7.72
110	.106283	1.18246	.190911	1.05799	.59457	15.485	8.4948	632	4477	1, 3, 9	8.01
120	.1062828	1.18199	.19072	1.0673	.58527	15.384	8.4855	650	4636	1, 3, 9	8.27
130	.106275**	1.18188	.19068	1.0693	.58319	15.361	8.4834	684	4869	1, 3, 9	8.72

\*Converged within 1% of the optimum point after approximately 25 bases.

\*\*Optimum point.



of function evaluations required for convergence. It demonstrates the ability of the BT procedure to move efficiently along a difficult behavior boundary.



## CHAPTER 5

### COMPARISON STUDY

The CADOP4 code as described in section 4.3.1 was used in this study along with all the constants and parameters presented earlier.

This comparison study is based on the works of Eason and Fenton given in References [14] and [15]. All ten problems treated in these references were run, using the new code with the starting points given in Reference [14]. All the control constants and the step sizes are internally generated so that there was no special tuning for individual problems. Computations were performed in double precision on an IBM 370 model 168 system, using a level G compiler, thus closely simulating the Eason and Fenton study.

A brief description of the codes studied are given in Table 3, while Table 4 contains the data for rating the success of the various codes in solving the ten problems to which they were applied. A detailed description of the problems is given in Reference [14]. A normalized time required for the solution of each problem successfully solved is given in Table 4. Normalized time is defined here as the execution CPU time divided by the CPU time required to execute a timing standardization program [14]. The symbol "P" denotes progress toward a solution, and a blank denotes failure. The criteria used in References [14] and [15] for defining successful solution or progress were also applied here.

TABLE 3  
CODE DESCRIPTIONS

Name	Description	Algor Class*
ADRANS	Random search followed by pattern moves	DS
CLIMB	Rosenbrock search	DS
DAVID	Davidon-Fletcher-Powell with numerical derivatives	GF
DFMCG	Fletcher-Reeves conjugate gradient method with secant approximation derivatives	G
DFMFP	Davidon-Fletcher-Powell with secant approximation derivatives	G
FMIND	Hook & Jeeves pattern search	DS
GRAD4	Steepest descent method	G
GRID1	Grid and star network search, with shrinkage	AR
MEMGRD	Davidon-Fletcher-Powell with retained step length information	GF
NMSERS	Simplex search	DS
PATSH	Modified pattern search, dome strategy	DS
PATRNI	Modified pattern search, ridge strategy	DS
RANDOM	Random search with shrinkage	AR
SEEK1	Pattern search followed by random search	DS
SEEK3	Modified pattern search	DSF
SIMPLX	Modified simplex search	DSF
DSDA	Modified pattern search followed by Mugele's search	DS
CADOP2	Modified pattern search followed by Zoutendijk feasible direction method	DS
CADOP3	Modified CADOP2	DS
CADOP4	Boundary Tracking method	BT

\*DS = direct search, DSF = direct search employing SUMT strategy and penalty function, G = gradient procedure, GF = gradient procedure using SUMT strategy and penalty function, AR = area reduction method, BT = Boundary Tracking.

TABLE 4  
PERFORMANCE OF OPTIMIZATION CODES\*

Problem No.	1	2	3	4	5	6	7	8	9	10
Variables	5	3	5	4	2	2	3	2	2	4
Constraints**	10	2	6	0	0	1	2	0	6	0
Code Names										
ADRANS	2.64	0.458	1.65	P	0.100	0.654	0.159	0.069	P	P
CLIMB				0.015	0.005			0.007		
DAVID		0.188	0.84	1.132	0.075	0.046				
DFMCG			P	0.015	P			0.004		
DFMFP			P	0.038	0.250		P	0.387		
FIND		0.004	P		0.140		0.003	0.003	P	3.74
GRAD4		P	P		0.393		P	0.004		P
GRID1	P	P		0.283	P	P		0.037	P	P
MEMGRD		0.143	0.91	0.059	0.066	0.067	P			
NMSERS		0.019	0.045	0.060	0.002	0.012	P	0.007	0.39	P
PATSH	1.78	0.220	1.00	0.013	0.018	0.020	0.010	0.009	P	3.54
PATRNO	P	P	P	0.021	P			0.002	P	1.95
PATRN1	P	P	P	0.008	0.002	P		0.001	1.02	1.20
RANDOM		P		P		0.024	1.20	0.013	P	P
SEEK1		P	P		0.010		0.010	0.007	P	1.53
SEEK3		0.102	0.14	0.212	0.035	0.191	0.141	0.013	4.20	P
SIMPLX	2.97	0.297	1.31	0.196	0.035	0.191	0.262	0.050	P	
DSDA	P	0.021	0.047	0.104	0.003	0.008	0.145	0.004	1.94	1.35
CADOP2	0.307	0.016	0.090	0.075	0.008	0.011	0.069	0.003	1.55	1.73
CADOP3	0.119	0.006	0.030	0.080	0.004	0.011	0.025	0.005	1.00	1.60
CADOP4	0.044	0.003	0.0125	0.080	0.004	0.005	0.003	0.005	0.39	1.60

\*Numerical entry indicates normalized time required for solution, and P indicates progress toward a solution [14, 15].

\*\*Excluding regional constraints.



The important variables effecting execution time are; the problem, the algorithm, the code, the input and output requirements, the architecture of the machine and the compiler system. In order to minimize the effects of those variables not involved in the comparison, similar computer machines and compiler systems along with the same test problems and output requirements are used here. Unfortunately the effects of the code structure can not accurately be determined. Thus, data of Table 4 and ratings shown in Table 5 can not be considered to accurately reflect the effectiveness of the basic optimization algorithms.

The data and rating procedures used here however, can be directly applied, with reasonable accuracy, for relative comparison of the codes tested. The results obtained are thus useful to the user of such codes. The relative effectiveness of basic optimization algorithms can only be inferred from this data if one assumes that the codes for each procedure have been prepared with essentially comparable effectiveness.

This study uses Eason and Fenton's comparison procedures since they are the best available and the most current. Furthermore, use of another investigator's comparison methods rather than one proposed by the developer of a new method reduces the tendency toward developer bias in reporting on the effectiveness of his method.

The data from Table 4 may be applied to a number of rating methods for comparing the codes tested. Table 5 presents relative ranking of



TABLE 5  
RELATIVE RANKING OF OPTIMIZATION CODES

	Generality		Efficiency		Generality and Efficiency
	$n_a$	$N_a$	$f_a$	$\bar{f}_a$	$T_a$
10	CADOP4 CADOP3 CADOP2	10 CADOP4 CADOP3 CADOP2	1.3 PATRN1	0.18 NMSERS 0.19 CADOP4	2.2 CADOP4 2.9 CADOP3 4.1 CADOP2
9	DSDA PATSH	9.5 DSDA PATSH	2.5 CADOP4	0.26 CADOP3 0.28 PATRN1	9 DSDA
8	SEEK3 SIMPLX	8.5 SEEK3 SIMPLX ADTRANS	3.8 CADOP3	0.40 CADOP2	15 PATSH
7	ADTRANS NMSERS	8.0 NMSERS	4.1 NMSERS	0.54 DSDA	16 NMSERS PATRN1
5	PATRN1 FMIND MEMGRD DAVID	7.0 PATRN1 FMIND SEEK1	6.6 CADOP2	0.82 MEMGRD	18 SEEK3
4	SEEK1	5.5 MEMGRD PATRN0	9.5 DSDA	0.85 PATSH	21 SIMPLX
3	CLIMB DFMFP GRAD4 PATRN0 RANDOM	6.0 FMIND SEEK1	15.7 FMIND	0.97 FMIND	24 ADTRANS
2	DFMCG GRID1	5.5 MEMGRD PATRN0	23.8 PATSH	1.2 SEEK3	25 FMIND
		DAVID GRAD4 GRID1 RANDOM	24.7 SEEK3	1.9 SIMPLX	26 MEMGRD
		5.0 GRID1 RANDOM	34.8 MEMGRD	2.4 DAVID	27 DAVID
		4.0 DFMFP	61.1 SIMPLX	2.9 ADTRANS	
		3.0 CLIMB DFMCG	63.6 DAVID 92.5 ADTRANS		

the codes using the criteria of Reference [15]. The rating equations are as follows:

Let the number of problems solved by code "a" be  $n_a$ , and let  $n'_a$  be the number of problems with a "P" rating. Then the numerical success rating  $N_a$  is given by

$$N_a = n_a + n'_a/2 \quad (5.1)$$

One of two computational efficiency ratings is given as

$$f_a = [\sum_{p=1}^{10} b_{ap} t_{ap} / \min(t_{ap})] / n_a \quad (5.2)$$

where  $b_{ap} = 1$  if code "a" solved problem "p" and zero otherwise,  $t_{ap}$  is the normalized time required for solution and  $\min(t_{ap})$  is the shortest time required by any of the codes studied to solve problem "p". The other efficiency criterion is

$$\bar{f}_a = [\sum_{p=1}^{10} b_{ap} t_{ap} / \text{mean}(t_{ap})] / n_a \quad (5.3)$$

where  $\text{mean}(t_{ap})$  is the average time required by the codes studied to solve problem "p". An overall rating number which can be considered a composite measure of generality (reliability) and efficiency (speed) is given by

$$T_a = \sum_{p=1}^{10} t'_{ap} \quad (5.4)$$

where  $t'_{ap}$  is set equal to  $t_{ap}$  if algorithm "a" solves a problem "p", and to twice the time used by the slowest code solving a problem "p" if code "a" could not solve it. This penalty time is used to penalize code unreliability. Only codes that solved half or more of the problems are rated for efficiency.

The tables presented here are similar to those given in References [15] and [17], except that the CADOP3 and CADOP4 codes are included.

The CADOP3 code is a modified version of CADOP2 code presented in Reference [17]. Thus, the rating methods and presentation of results used are essentially those of Reference [15] and [17].

From Tables 4 and 5 it can be concluded that CADOP4 is the fastest code in overall generality and efficiency rating. This Boundary Tracking method presented here appears comparable in speed to the fastest methods presented in Reference [17], (NMSERS, PATRNI, DSDA, and CADOP2). CADOP4 is faster than average in all problems. It is the fastest code solving problems 1, 2, 3, 6, 7, and 9, which are problems with behavior constraints. On the other hand, problems 4, 5, 8, and 10, where the CADOP3 and CADOP4 codes performed identically, but less efficiently than some other procedures, are problems without such constraints. This is expected since the two codes are identical in treating the unconstrained problems.

Of the problems tested, problem 1 which has the largest number of behavior constraints (10) was apparently also the most difficult, since it was solved by only six of the twenty-one codes presented in Table 4. The second most difficult problem was problem 9, for which only 7 of the 21 codes led to the optimum point. This problem has only 6 behavior constraints and two variables. However, there is a rapid change in the slope of the behavior boundary in the region near the optimum point. Because of this rapid variation in slope, a major part of the total execution time was spent on refining the location of the point so as to meet the convergence criterion. Problem 10, which required the longest execution time, has no behavior constraints. The long execution time



required by this problem is due to the complexity of the objective function and the number of the function evaluations needed to reach the optimum.

It can be seen from Table 4 that the CPU time required for treating problems 9 and 10 in most cases is much greater than the sum of the CPU times required for the solution of the rest of the problems tested. Thus, the speed of a code in solving problems 9 and 10 plays an overwhelming role in determining the code's overall generality and efficiency rating,  $T_a$ . For example, a code that is very efficient on the majority of problems but requires long solution times for problems 9 and 10 would have a relatively low overall generality and efficiency rating using equation (5.4). Therefore, this rating method is not very useful for comparing codes solving all the test problems. For such codes the efficiency ratings  $f_a$  and  $\bar{f}_a$  represent the ability of the method more clearly. Furthermore, the overall generality and efficiency rating  $T_a$  does not sufficiently penalize those codes which failed to solve any of the test problems 1 through 8, but performed well on problems 9 and 10. The penalty time used here fails to accurately take into account the weaknesses of such codes in solving problems 1 through 8.

The superior performance of CADOP4 code in problems with behavior constraints compared to CADOP3 code is due to the fact that the number of function evaluations required in CADOP3 is proportional to the number of bases needed for solution multiplied by the number of variables. On the other hand, the number of function evaluations in CADOP4 is



proportional only to the number of base points, and does not have to be multiplied by the number of variables. Therefore, in CADOP3 the number of function evaluations increases directly with the number of variables, while in the CADOP4 code it does not.

Compared to the relatively reliable codes ( $n_a > 8$ ), CADOP4 is faster than CADOP3 on six of the ten problems solved by CADOP3, faster than DSDA on six of nine, and faster than PATSH on eight of nine, and faster than SEEK3 in all problems solved by these schemes. As may be seen, the CADOP2 and CADOP3 codes are the only reliable codes comparable to CADOP4. CADOP4 is significantly faster than CADOP3, CADOP2, PATSH, SEEK3, and SIMPLX. The straight pattern (PATRN1) or simple (NMSERS) codes are ranked relatively high in efficiency primarily due to their superior performance in unconstrained problems (Table 5). Of this group, only NMSERS appears to be sufficiently reliable to merit consideration for use. The minor difference in efficiency between NMSERS and CADOP4 is, however, overshadowed by the superior reliability of the latter. Thus, in the overall speed, generality, and efficiency rating, CADOP4 stands out. Viewed on the basis of these comparisons, CADOP4 appears to be a superior nonlinear mathematical programming code.

The new algorithm is intended to be a constrained optimization algorithm. Therefore, the performance of CADOP4 is compared to the codes of References [15] and [17] on problems having behavior constraints. This comparison is shown in Table 6.

Table 6 is similar to Table 5 except that the problems without

TABLE 6  
RANKING OF OPTIMIZATION CODES IN PROBLEMS WITH BEHAVIOR CONSTRAINTS

	Generality		Efficiency		Generality and Efficiency
	$n_a$	$N_a$	$f_a$	$\bar{f}_a$	
6	CADOP4 CADOP3 CADOP2	6 CADOP4 CADOP3 CADOP2	1.0 CADOP4	0.07 CADOP4	0.46 CADOP4 1.2 CADOP3
5	DSDA	DSDA	3.2 CADOP3	0.15 NMSERS	2.0 CADOP2
	PATSH	PATSH	3.3 NMSERS	0.19 CADOP3	
	SEEK3	5.5 SIMPLX	8 CADOP2	0.43 CADOP2	8.1 DSDA
	SIMPLX	ADTRANS	13 DSDA	0.83 DSDA	10.7 SEEK3
4	ADTRANS	5 SEEK3			
3	NMSERS	4.5 NMSERS	28 SEEK3	1.0 PATSH	11.4 PATSH
	MEMGRD	3.5 MEMGRD	39 PATSH	1.1 MEMGRD	13.4 SIMPLX
2	DAVID	PATRN1	43 MEMGRD	1.2 DAVID	14 ADTRANS
1	FMIND	3 SEEK1	63 DAVID	1.3 SEEK3	17 NMSERS
	RANDOM	DAVID	78 SIMPLX	2.1 SIMPLX	18 MEMGRD
0	PATRN1	2.5 RANDOM	10.4 ADTRANS	3.2 ADTRANS	18 DAVID
	SEEK1				
	CLIMB				
	DFMFP	PATRN0			
	GRAD4	2 GRID1			
	PATRN0	1.5 GRAD4			
	DFMCG	1 DFMFP			
	GRID1	0.5 DFMCG			
		0 CLIMB			

behavior constraints are excluded. The rating equations used for these values are the same as those used for Table 5. The results of Table 6 indicate the superiority of CADOP4 with respect to speed, generality, and efficiency. Only codes that solved half or more ( $n_a \geq 3$ ) of the problems are rated for efficiency.

The superior performance of the CADOP4 code in all the above ratings strongly suggests the superiority of the BT method for treating problems with behavior constraints. CADOP4 proved to be substantially more efficient than the CADOP3 and NMSERS codes on such problems. In the overall generality and efficiency rating CADOP4 code again stands alone with CADOP3 code in the second place being approximately three times slower. However, as explained earlier, due to the relatively long execution time required for problem 9 this rating method does not reflect accurately the relative effectiveness of the codes which solved all the test problems. The efficiency ratings  $f_a$  and  $\bar{f}_a$  may again be more useful in comparing such codes. In these ratings CADOP4 code is two to three times faster than other relatively fast codes (CADOP3, NMSERS).

Thus, the Boundary Tracking algorithm presented here appears to be superior to DSFD with regard to efficiency and to all other optimization procedures tested with respect to generality and efficiency.

Based on its performance on the ten problems of Reference [15] and on the other comparison studies, the Boundary Tracking method appears to be a fast and reliable nonlinear mathematical programming optimization procedure.



In conclusion, it must be pointed out that the test problems used in the above comparison study are relatively small and simple, while many practical engineering problems are large and contain complex and computationally demanding functions. Therefore, although it is reasonable to assume that the above comparison study is representative of the performance of the new code on most practical problems of size and complexity similar to that of the study, this performance may not be representative for large complex problems. Unfortunately, no comparison study utilizing large complex problems is available, and is not likely to be available soon due to the difficulty and cost associated with such a project. Furthermore, one cannot guarantee that the performances noted in the present study are typical for all relatively small simple problems. Nevertheless, this is the most complete of the available general comparison studies and should be useful as a guide in selecting a suitable algorithm for a particular problem. The designer must, however, proceed with care in comparing his problem to the above test problems, taking into account such things as the number of variables, constraints, nature of the function to be evaluated, etc. in selecting a desirable algorithm.

## CHAPTER 6

### CONCLUSION

The successful application of the CADOP4 code to the relatively complex problem of shell synthesis and its performance in the general comparison study presented in section 4.1, imply that the Boundary Tracking method developed here is a superior nonlinear mathematical programming procedure. Although the code proved to be the best in the general comparison study, the real potentials of the algorithm are demonstrated in the shell design problem. Since many engineering problems are of such a class, the new algorithm shows the promise of adding a major contribution to the field of automated design.

In the above studies the BT method proved to have great potential for use in computationally demanding problems. However, as in the case of most new methods, additional studies may lead to improvement, particularly in the speed of the algorithm.

The only apparent disadvantage of CADOP4 is its relative complexity compared to some of the other reasonably reliable methods. It contains 1320 FORTRAN statements, while, for example, the CADOP3 contains 790, DSDA contains 372, and PATSH only 75 FORTRAN statements. Thus, if CADOP4 code is not available in a compiled form, for simple problems of relatively low complexity and dimensionality, one of the simpler codes may be preferable since the time required for compilation of the program may exceed the time saved by using CADOP4.

In addition, its performance on problems without behavior constraints, although quite good, is not as outstanding as on problems with such constraints.

In conclusion, the user of this or any other algorithm for automated design, should be aware that the general nonlinear constrained optimization problem is quite difficult to handle. Also, none of the available techniques will guarantee an optimum solution. One should, therefore, be careful in the application of such an algorithm and analyze the results thoroughly. One also, should make use of several synthesis runs, using different starting points where possible, before assuming the value is an optimum solution.



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## USER INSTRUCTIONS FOR CADOP4

I. INSTRUCTION

This code treats inequality constrained or unconstrained linear or nonlinear minimization problems by means of a direct search mathematical programming method. The method starts from a user specified starting or initial point and generates a sequence of better points until, hopefully, an optimal, or near optimal, point is reached. The code is intended primarily for constrained nonlinear problems. Linear problems are much more effectively handled by one of many linear programming methods. Unconstrained problems are better treated by UNCDP, a simplified version of CADOP2, or one of several other unconstrained nonlinear problem codes. CADOP4 will, however, treat both linear and unconstrained problems.

It should be noted that nonlinear mathematical programming methods generally do not guarantee an optimal solution because of the possibility of multiple local optima, algorithm failure or numerical difficulties. Although CADOP4 is among the most reliable of the nonlinear mathematical programming codes it cannot be considered absolutely reliable. Thus, it is desirable to use several optimization runs with widely separated starting points to confirm the convergence has been achieved or to determine if local optima are present.



## II. PROBLEM FORMULATION

This code treats the problem:

Find those values  $\bar{x}_i$  of the set of "variables"  $x_i$ ,  
 $i = 1, 2, \dots, IP$  and the constant "parameters"  $p_k$ ,  $k = 1, 2, \dots, KP$ ,  
 that result in the minimum value of the objective function  
 $f(p_k, x_i)$ , that is

$$f(p_k, \bar{x}_i) = \min [f_k(p, x_i)] \quad (1)$$

while also satisfying the "behavior" constraints

$$g_j(p_k, x_i) \geq 0 \quad j = 1, 2, \dots, JP \quad (2)$$

and the "regional" constraints

$$x_i^l \leq x_i \leq x_i^u \quad (3)$$

The program in its present form treats problems with

$$2 \leq IP \leq 10, \quad 0 \leq JP \leq 10 \quad \text{and} \quad 0 \leq KP \leq 100$$

### III. SPECIFICATION OF OBJECTIVE AND CONSTRAINT FUNCTIONS

The subprogram FUNCTION OBJ(J) is essentially a dummy subprogram created to accept the users FORTRAN IV program statements defining the objective and behavior constraint functions. The normal form of the behavior constraints is

$$B_j(p_k, x_i) \leq U_j(p_k, x_i) \quad (4)$$

where  $B_j$  can be thought of as the behavior and  $U_j$  the upper limit of behavior.

The FUNCTION OBJ(J) is modified so as to define the objective and constraint functions by inserting the following statements immediately after the COMMON statement

```
GO TO (1,2,---jp), J      (omit if no constraints are used)
OBJ = expression defining f (pk, xi) using arrays P(k), X(i)
RETURN
j B = expression defining Bj
U = expression defining Uj
GO TO 101
```

A constraint statement group is used for every constraint. The last constraint group need not use the final GO TO statement.

Example

For the problem:

minimize

$$2x_1 x_2 - p_1 x_3 x_4^2$$

such that

$$2x_3^3 - x_1 \leq p_2$$

and

$$-6 \leq x_2^2 - x_4 \leq 0$$

one could define three constraints and insert the statements

GO TO (1,2,3), J

OBJ = 2. \* X (1) \* X (2) - P (1) \* X (3) \* X (4) \*\*2

RETURN

1 B = 2.\* X (3) \*\* 3 - X (1)

U = P(2)

GO TO 101

2 B = X(2)\*\* 2 - X(4)

U = 0.

GO TO 101

3 U = (X (2) \*\* 2 - X (4) )

B = - 6.



Alternately, noting that both upper and lower limits on the second constraint equation cannot be active simultaneously one could use two constraint equations and insert the program segment:

```

GO TO (1,2),J
ORJ = 2. * X (1)* X(2) - P (1) * X (3) * X (4) ** 2
RETURN
1 B = 2. * X (3) ** 3 - X (1)
  U = P(2)
  GO TO 101
2 TB = X (2) ** 2 - X (4)
  LF(TB.LT.-3.) GO TO 3
  B = TB
  U = 0
  TO TO 101
3 B = -6.
  U = TB

```

The constraints values at the optimum are printed in the form of equation (2) where

$$g_j = \begin{cases} -(B_j - U_j)/|U_j| & U_j \neq 0 \text{ and } B_j \neq 0 \\ -(B_j - U_j) & U_j = 0 \text{ or } B_j = 0 \end{cases}$$

thus a positive value of  $g_j$  indicates the constraint is satisfied.

#### IV DATA CARDS

The program allows multiple optimization runs of a particular problem within a single computer run using different parameters, for parametric studies, different starting points, for optimality confirmation or search for local optima, and different sets of regional constraint limits.

The user must, by use of the data card set, specify the number of parameters, variables and behavior constraints used. specify for the first run if regional constraints are to be used, and for subsequent runs whether the parameters, initial point or regional limits are to be changed. If parameters are used they must be entered. The initial point must be entered. The values for the regional constraints must be entered if such limits are imposed.

The first data set is entered on the "Problem Constraints" card which specifies, in order, the number of parameters (KP), variables (IP) and behavior constraints (JP), used (see line 8 of program listing). The data is entered in 3I10 format in the first three fields in order and must be right justified.

The 2nd data set is entered on the "Data Control" card and is used to specify whether: 1) new parameters are to be used (ICNTR2), 2) a new initial point is to be used (ICNTR3) and, 3) regional limits or new regional limits are to be used (ICNTR4) (see lines 12-23). The entries are made in 3I10 format in the order given above. For the first run no entries in

the first two fields are needed. If regional limits are used an entry, any nonzero digit, is made in the third field (col. 21-30).

If, and only if, the number of parameters specified is greater than zero ( $KP > 0$ ) a 3rd data set is used to enter the problem parameters  $p_k$ . The entries are made 5 to a card in F15.5 format in order  $i = 1, 2 \dots KP$ , (see lines 13 and 14).

The 4th data set specifies the starting point and entries are made, in order, 8 to a card in F10.5 format (see lines 7 and 15).

If, and only if, an entry is made in the third field of the Data Control card ( $ICNTR4 \neq 0$ ) a 5th data set defining the lower limits is entered, 8 to a card, in F10.5 format followed by an upper limit set (starting with a new card) with similar format. Both complete limit sets must be entered (see lines 22-25).

For every additional run an additional Data Control card is added followed by parameter and/or initial point and/or regional limit sets, where and only where the need for a new set is indicated by an appropriate entry ( $ICNTR2 \neq 0$  or  $ICNTR3 \neq 0$  or  $ICNTRL4 \neq 0$ ) on the Data Control card (see lines 18-22).

A blank Data Control card is used to terminate the run(s) (see lines 18 and 19).



## V. CONVERSION TO SINGLE PRECISION

The program as supplied is a double precision form. Experience has shown, however, that the great majority of problems can be treated adequately in single precision and thus it is recommended that single precision be tried first. To convert to single precision, remove the IMPLICIT statement at the beginning of MAIN and all subprograms. Insert function conversion statements such as  $DSQRT(B) = SQRT(B)$ , etc. after the COMMON block in the subprograms where such functions are used. Furthermore, the REAL FUNCTION OBJ\*8(J) should be put in single precision form.

Storage requirements for the basic program in double precision is about 150K and in single precision about 100K.

## VI. CHANGE OF PROBLEM SIZE

To change the maximum number of variables (IP) or the maximum number of constraints (JP) the program can treat, change the arrays in MAIN and all subprograms as follows:

1. Change arrays of the COMMON statements of the main and all subprograms as follows;

D, DL, DU, and DZ become D(IP), DL(IP), DU(IP) and DZ(IP).

XB becomes XB(IP,5).

V(A in OPT2, CONMOV and LINPRO) becomes V(M,N). Where

$$M = JP + 4IP + 5$$

$$N = JP + 5IP + 6$$

GN (GO in OPT2, CONMOV, ZERO, and G in PATTRN and FIND)

becomes GN(JP). IA becomes IA(JP).

where IP is the new maximum number of variables and JP the new number of constraints

2. In COMMON/DOL/ change BL array to BL(JP) wherever this statement is used.
3. In COMMON/ZE/ change DT and DTT to DT(IP) and DTT(IP).  
change SE to SE(JP).  
change DK to DK(JP + 1, IP).
4. In COMMON/POL/ change GB to GB(JP).
5. In COMMON/CON/ change SS to SS(IP).  
CHANGE IJ and JI to IJ(JP) and JI(JP).
6. In COMMON/FIN/ change x to x(IP).  
change IA, CK and IC to IA(JP), CK(JP) and IC(JP)

7. In the SUBROUTINE DELF Dimension statement change DT and DTT to DT(IP), DTT(IP) and GO to GO(JP).
8. In the SUBROUTINE DB DIMENSION statement change DT to DT(IP).
9. In the OPT2 SUBROUTINE DIMENSION statement change IB, IC, and X to IB(IP) etc., TN and GG to TN(JP), GG(JP). change SSS to SSS(M), where M is defined in item 1 as DB1 to DB1 (JP + 1, IP).
10. In the SUBROUTINE CONMOV DIMENSION statement change GG to GG (JP) and X to X (IP)
11. In the SUBROUTINE ZERO DIMENSION statement change GG to GG (JP).
12. In the SUBROUTINE FIND DIMENSION statement change DT(10) to DT(IP).
13. In the SUBROUTINE PATTERN DIMENSION statement change all 10's to IP.
14. Change all dummy arrays such as DUM, IDUM, IDUN, etc. in all COMMON statements to equalize COMMON size.



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MAIN

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```

0001 IMPLICIT REAL*8(A-H,I-Z)
0002 COMPEN D(10),P(100),DL(10),DU(10),OZ(10),A,XB(10,5),GR(10),FB(5),
      CV(5,66),Q,IP,KP,JP,LDUN(22)
0003 COMMON IXJ
0004 FORMAT(5F15.5)
0005 FORMAT(4I10)
0006 FORMAT(2F10.5)
0007 FORMAT(8F10.5)
0008 READ2,KP,IP,JP
0009 DO 21 I=1,IP
0010 DL(I)=-1.E+48
0011 DU(I)=1.E+48
0012 READ2,ICNTR2,ICNTR3,ICNTR4
0013 IF(KP.EQ.0) GO TO 12
0014 READ1,(PI),I=1,KP
0015 READ101,(D(I),I=1,IP)
0016 FORMAT(1H0,' * STARTING DESIGN VARIABLE VALUES * ')
0017 GO TO 23
0018 READ(5,2,END=33)ICNTR2,ICNTR3,ICNTR4
0019 IF(ICNTR2+ICNTR3+ICNTR4.EQ.C)STOP
0020 IF(ICNTR2.NE.O)READ1,(P(I),I=1,KP)
0021 IF(ICNTR3.NE.O)READ101,(D(I),I=1,IP)
0022 IF(ICNTR4.EQ.0)GO TO 22
0023 READ 101,(DL(I),I=1,IP)
0024 FORMAT(1H0,' * LOWER LIMITS OF DESIGN VARIABLES * ')
0025 READ 101,(DU(I),I=1,IP)
0026 FORMAT(1H0,' * UPPER LIMITS OF DESIGN VARIABLES * ')
0027 IF(KP.LE.0) GO TO 104
0028 PRINT 6
0029 PRINT7,K,P(K),K=1,KP)
0030 PRINT 18
0031 PRINT101,(D(I),I=1,IP)
0032 PRINT 17
0033 PRINT101,(DL(I),I=1,IP)
0034 PRINT 19
0035 PRINT101,(DU(I),I=1,IP)
0036 CALL DELF(FOPT)
0037 PRINT 180,FUPT
0038 198 FORMAT(' * OPTIMUM DESIGN=',F15.9)
0039 180 FORMAT(' *DESIGN PARAMETERS')
0040 6 FORMAT(' P',I2,'=',F14.4)
0041 PRINT8
0042 FORMAT(' *DESIGN VARIABLE VALUES*')
0043 PRINT9,K,D(K),K=1,IP)
0044 FORMAT(' D',I1,'=',F15.8)
0045 IF(JP.EQ.0) GO TO 24
0046 PRINT10
0047 FORMAT(' *ONEARNESS TO CONSTRAINTS*')
0048 PRINT 11,(GN(K),K=1,JP)
0049 FORMAT(' C',I2,'=',F15.5)
0050 11 GO TO 24
0051 100 STOP
0052 33 END

```

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```

0001 SUBROUTINE DELF(FDPT)
0002 IMPLICIT REAL*8(A-F,H-Z)
0003 COMMON D(10),P(100),OL(10),DU(10),DZ(10),A,XB(10,5),GH(10),FB(5),
0004 CV(55,66),C,IP,KP,JP,1DUN(22)
0005 COMMON IXJ
0006 COMMON/DOL/STEST,TDIF,AXI,AMIN,BL(10),AQ,IN
0007 COMMON/PAT/DRJ,JE,IAY2
0008 DIMENSION GO(10),OT(10),OTT(10)
0009 IXYZ=1
0010 KT=0
0011 STEST=0.
0012 IN=0
0013 AD=1.
0014 K=1
0015 A=1.
0016 AXI=1.
0017 FTST=0.
0018 TDIF=0
0019 JK=0
0020 LI=0
0021 IAJ=0
0022 IF(JP.EQ.0) GO TO 51
0023 DO 3 I=1,JP
0024 BL(I)=1.
0025 GO(I)=10.
0026 K=1
0027 IF(LI.GT.0) GO TO 31
0028 CU 5 J=1,JP
0029 CN(J)=DBJ(J)
0030 CONTINUE
0031 FE(K)=DBJ(0)
0032 IF(LI.EQ.1) AXI=10.*AXI
0033 CALL DB(0,LI)
0034 IF(JP.EQ.0) GO TO 1000
0035 PRINT 514,(D(I),I=1,IP),FB(K)
0036 FORMAT(12F10.5)
0037 IF(KT.EQ.0) GO TO 45
0038 DIF=DABS((FTST-FB(1))/FB(1))
0039 IF(DIF.GT. 1.E-15) GO TO 45
0040 IF(DIF.GT.TDIF) GO TO 45
0041 FDPT=FB(K)
0042 RETURN
0043 IF(A.LT.AMIN) GO TO 1771
0044 KT=KT+1
0045 IF(KT.EQ.10) GO TO 1000
0046 TDIF=0.1F
0047 FTST=FB(1)
0048 SUN=0.
0049 GO 81 I=1,IP
0050 SUN=SUN+DZ(I)*2
0051 SUN=DSQRT(SUN)
0052 IF(SUN.EQ.0) GO TO 1771
0053 CONTINUE
0054 IF(A.GT.AMIN) GO TO 5120
0055 FDPT=FB(K)
0056 RETURN

```

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DELF

FORTTRAN IV G LEVEL 21

```

0056 5120 AL=A
0057 14 SUMM=0.
0058 DU 82 I=1,IP
0059 DT(1)=D(1)
0060 XD(1,K)=D(1)
0061 8 D(1)=D(1)-DZ(I)*AL/SUM
0062 IF(D(1)-DT-DU(1)) D(1)=DU(1)
0063 IF(D(1)-LT-DL(1)) D(1)=DL(1)
0064 82 SUMM=SUMM+(D(1)-DT(1))*2
0065 SUMM=DSORT(SUMM)
0066 IF(SUMM-EQ-0) GO TO 1771
0067 DU 83 I=1,IP
0068 C(1)=DT(1)+(D(1)-DT(1))*AL/SUMM
0069 IF(D(1)-GT-DU(1)) D(1)=DU(1)
0070 IF(D(1)-LT-DL(1)) D(1)=DL(1)
0071 83 CONTINUE
0072 I*J=0
0073 IF(JP-EQ-0) GO TO 12
0074 I=0
0075 DU 9 J=1,JP
0076 GU(J)=GN(J)
0077 GN(J)=DL(J)
0078 IF(GN(J)-GT-0.) GO TO 9
0079 I=I+1
0080 CONTINUE
0081 IF(I) 12,12,13
0082 12 K=K+1
0083 FC(K)=DS(J(O))
0084 DU 1818 L=1,IP
0085 XB(L,K)=D(L)
0086 IF(FB(K)-GT-FB(K-1)) GO TO 19
0087 IF(LI-GT-0) GO TO 1401
0088 18 ZL=2.*AL
0089 IF(K-LT-5) GO TO 14
0090 FB(1)=FB(K-2)
0091 FB(2)=FB(K-1)
0092 FB(3)=FB(K)
0093 DU 141 I=1,IP
0094 XB(I,1)=XB(I,K-2)
0095 XB(I,2)=XB(I,K-1)
0096 XB(I,3)=XB(I,K)
0097 141 CONTINUE
0098 K=3
0099 GU TO 14
0100 13 K=K+1
0101 DU 15 N=1,IP
0102 XB(N,K)=D(N)
0103 KU=0
0104 KS=1
0105 GSS=GN(1)
0106 DD 17 J=2,JP
0107 IF(GSS-LT-GN(J)) GO TO 17
0108 GSS=GN(J)
0109 KS=J
0110 17 CONTINUE
0111 J=KS

```



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DELF

FCRTRAN IV G LEVEL 21

```

0112 DD 23 L=1,IP
0113 DT(L)=XB(L,K-1)
0114 DT(L)=XG(L,K)
0115 IF(DABS(GN(J)).LE-.000001) GO TO 1701
0116 GS=GO(J)
0117 T=GS/(GS-GSS)
0118 CONTINUE
0119 DD 24 L=1,IP
0120 DL)=DT(L)+T*(DT(L)-DT(L))
0121 IF(D(L)-LT-DL(L)) D(L)=DL(L)
0122 IF(D(L)-GT-DL(L)) D(L)=DU(L)
0123 IXJ=0
0124 GN(J)=DBJ(J)
0125 IF(DABS(GN(J)).GT-.000001) GO TO 100
0126 GO TO 170
0127 GS=GSS
0128 GSS=GN(J)
0129 DD 1021 L=1,IP
0130 DT(L)=DT(L)
0131 DT(L)=D(L)
0132 GO TO 1031
0133 CONTINUE
0134 IXJ=0
0135 DD 716 J=1,JP
0136 GN(J)=DBJ(J)
0137 DBJ=GBJ(K)
0138 IF(K-LE-2) GO TO 1775
0139 IF(GBJ-GT-FB(K-1)) GO TO 1774
0140 GO TO 1775
0141 DD 1776 I=1,IP
0142 D(I)=XB(I,K-1)
0143 FUPT=FB(K-1)
0144 DD 16 J=1,JP
0145 GN(J)=GO(J)
0146 LI=0
0147 FUPT=GBJ
0148 CALL OPT2(FUPT,LI)
0149 IF(LI.GT.0) GO TO 5101
0150 RETURN
0151 FB(I)=FUPT
0152 GO TO 510
0153 FB(I)=FB(K-1)
0154 DD 191 I=1,IP
0155 D(I)=XB(I,K-1)
0156 LI=2
0157 K=1
0158 GO TO 51
0159 A=AJ
0160 CALL PATRN(KA,SB)
0161 IF(KA-EQ.0) GO TO 510
0162 FUPT=SB
0163 LI=0
0164 RETURN
0165 END

```

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DB

FORTRAN IV G LEVEL 21

```

0001 SUBROUTINE DB(J,LI)
0002 IMPLICIT REAL*8(A-H,O-Z)
0003 COMMON D(10),P(100),DL(10),DU(10),DZ(10),A,XH(10,5),CN(10),F8(5),
0004 CV(55,66),Q,IP,KP,JP,TDUN(22)
0005 COMMON IXJ
0006 COMMON/CBL/STEST,TDIF,AX1,AMIN,BL(10),AO,IN
0007 DIMENSION DT(10)
0008 IXJ=0
0009 TR=OBJ(J)
0010 IXJ=0
0011 DEL=.001
0012 IF(A-LT-DEL) DEL=A
0013 DO 1 I=1,IP
0014 DT(I)=D(I)
0015 D(I)=D(I)+DEL
0016 DZ(I)=(OBJ(J)-TN)/DEL
0017 IXJ=0
0018 DT(I)=DT(I)
0019 DTEMP=0.
0020 ITEMP=0
0021 GO 2 I=1,IP
0022 IF(DABS(DZ(I))-LT-DTEMP) GO TO 2
0023 DTEMP=DABS(DZ(I))
0024 ITEMP=I
0025 CONTINUE
0026 IF(LI-EO-2) RETURN
0027 A=AJ/AXI
0028 IF(JP-EO-0) GO TO 11
0029 DO 3 I=1,JP
0030 EL(I)=.1/AXI
0031 IF(LI-GT-0) RETURN
0032 A=DABS((O.OI-TN)/DZ(ITEMP))
0033 IF(A-LT-.01) A=-.01
0034 AO=A
0035 AMIN=A/1000.
0036 PRINT 10,A,AMIN
0037 FORMAT(2F10.5)
0038 RETURN
0039 END

```

AD-A039 094

NEW JERSEY INST OF TECH NEWARK

F/G 13/13

A FAST BOUNDARY TRACKING ALGORITHM FOR CONSTRAINED NONLINEAR MA--ETC(U)

MAR 77 J MORADI, M PAPPAS

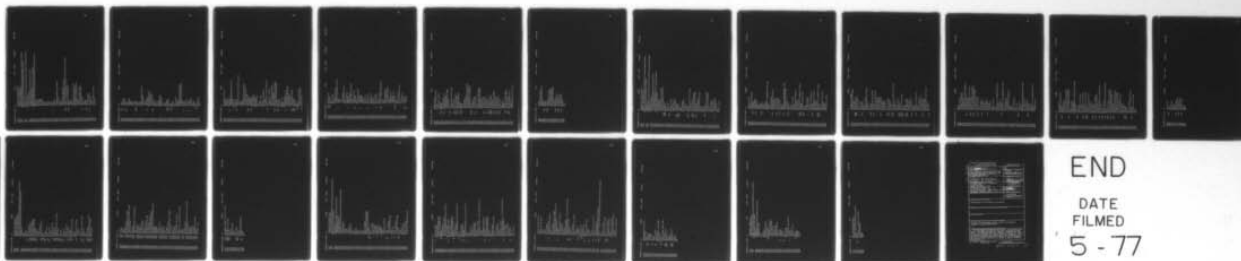
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GPT2

FORTRAN IV C LEVEL 21

```

0001 SUBROUTINE DPT2(FOPT,L1)
0002 IMPLICIT REAL*8(A-H,O-Z)
0003 INTEGER Z,E,G,BB,M,E,H
0004 COMMON D(10),P(100),DL(10),DU(10),DZ(10),V,XB(10,5),GG(10),FB(5),
0005 CA(55,66),Q,IP,KP,JP,IA(10),KL,KW,M,L,B,BB,E,G,Z,H,M
0006 COMMON IXJ
0007 COMMON/ZE/GS,GSS,SE(10),DK(11,10),DT(10),DTT(10),DI,SMAL,JIN,K,HU,
0008 C1M,JJ,J12,L11
0009 COMMON/PRL/G8(10)
0010 COMMON/DOL/STEST,TDIF,AXI,AMIN,BL(10),AD,JN
0011 COMMON/PAT/DBJ,JK,IXYZ
0012 COMMON/CON/SS(10),BASE,IJ(10),JT(10),J1Q,I2JUMP
0013 DIMENSION IB(10),IC(10),SS(55),TN(10),GG(10),X(10),DB1(11,10)
0014 BASE=1.
0015 SBASE=0.
0016 SS=FOPT
0017 JXN=1000
0018 JIN=1000
0019 JIX=0
0020 AL=V
0021 MU=0
0022 JIN=0
0023 JIN=0
0024 LI=0
0025 LI1=0
0026 JJ=1
0027 VT=V/10.
0028 ICC=0
0029 IF(1BASE-EQ-BASE) GO TO 3001
0030 SSASE=BASE
0031 JIN=0
0032 IF(IAL-EQ-V) GO TO 101
0033 PRINT 1500,V,FOPT,(D(1),I=1,IP)
0034 FORMAT(10X,10F10.5,10F10.5)
0035 PRINT 1501,(GG(J),J=1,JP)
0036 FORMAT(10X,10F10.5)
0037 SMAL=0
0038 SB=FOPT
0039 AL=V
0040 IF(1B-EQ-STEST) GO TO 150
0041 DIF=DABS(1B-STEST)/SB
0042 IF(DIF.GT. 1-E-J51) GO TO 45
0043 IN=IN+1
0044 IF(IN.LT.2) GO TO 150
0045 IF(DIF.GT-TDIF) GO TO 45
0046 FOPT=FB(1)
0047 LI=0
0048 RETURN
0049 V=V/2.
0050 DO 151 I=1,JP
0051 BL(1)=BL(1)/2.
0052 AX1=AX1*2.
0053 LI1=1
0054 IF(V-LE-AMIN) GO TO 46
0055 GO TO 47

```

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OPT2

FORTRAN IV G LEVEL 21

```

0055      45      IN=0
0056      47      STEST=SB
0057      TOIF=DIF
0058      101      JJ=1
0059      JK=1
0060      IZJUMP=0
0061      J2Q=0
0062      J3Q=0
0063      JU=1
0064      DI=10.
0065      3000      J12=1
0066      MU=0
0067      NU=0
0068      MP=0
0069      IF(V-CT-AMIN) GO TO 11
0070      FOPI=FB(JJ)
0071      LI=0
0072      RETURN
0073      11      DEL=-00001
0074      IF(V-LI-DEL) DEL=V
0075      IP1=JP+4*IP+4
0076      DO 103 I=1,IP1
0077      103      SSS(I)=0
0078      JK=1
0079      N=IP+1
0080      Z=-1
0081      MM=JP+1
0082      M=MM+2*IN+2*IP
0083      L=MM+N*IP
0084      E=0
0085      G=0
0086      NN=6
0087      90      Q=9999
0088      190      B=M+N*G+1
0089      W=M
0090      320      H=1
0091      BR=B+1
0092      J=0
0093      DO 4 I=1,IP
0094      18(I)=0
0095      IC(I)=0
0096      IF(D(I)-DL(I)-LT-V)GO TO 5
0097      IF(DU(I)-D(I)-LT-V)GO TO 6
0098      GO TO 4
0099      5      J=J+1
0100      18(I)=J
0101      GO TO 4
0102      J=J+1
0103      IC(I)=J
0104      4      CONTINUE
0105      JX=J
0106      MM=JP+1
0107      IL=0
0108      156      J=0
0109      DO 22 I=1,MM
0110      11=1-I

```

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FORTRAN IV 6 LEVEL 21          OPT2          DATE = 77068          PAGE 0003

0111 IF(I.NE.1) GO TO 78
0112 TM=FOPT
0113 FB(JJ)=TM
0114 GO TO 77
0115 CONTINUE
0116 IF(GO(11).GT.BL(11)) GO TO 22
0117 TM=GO(11)
0118 77 J=J+1
0119 TN(J)=TM
0120 CONTINUE
0121 22 IF(JX.EQ.JXN-AND.J.EQ.JIN) GO TO 113
0122 JIN=J
0123 JIM=J
0124 JXN=JX
0125 IF(JIM.EQ.JIN) GO TO 2000
0126 IF(JP.EQ.Q) GO TO 221
0127 DO 220 J=1,JP
0128 GB(J)=GO(J)
0129 DBJ=FB(JJ)
0130 CONTINUE
0131 DO 23 K=1,IP
0132 XB(K,JJ)=D(K)
0133 DT(K)=D(K)
0134 D(K)=D(K)+DEL
0135 J=0
0136 IXJ=0
0137 DU 24 I=1,MH
0138 II=I-1
0139 IF(I.EQ.1) GO TO 777
0140 IJ(1)=0
0141 IF(GO(11).GT.BL(11)) GO TO 24
0142 777 J=J+1
0143 IF(11.NE.0) IJ(11)=J
0144 JI(J)=11
0145 IF(ICC.NE.Q) GO TO 1000
0146 DB1(I,K)=CBJ(11)
0147 DK(J,K)=(DB1(I,K)-TN(J))/DEL
0148 IF(J.GT.1) DK(J,K)--DK(J,K)
0149 24 CONTINUE
0150 D(K)=DT(K)
0151 JIN=J
0152 DO 25 I=1,J
0153 SUM=0.
0154 DO 26 K=1,IP
0155 SUM=SUM+DK(I,K)*2
0156 IF(SUM.EQ.0.) GO TO 250
0157 SUM=DSORT(SUM)
0158 DO 27 K=1,IP
0159 DK(I,K)=DK(I,K)/SUM
0160 250 SE(1)=SUM
0161 25 CONTINUE
0162 JQ=0
0163 330 LX=W+2
0164 IF(J.GT.1) GO TO 775
0165 IF(JX.EQ.0) GO TO 152
0166 775 DO 350 I=1,LX

```



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OPT2

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FCRTRAN IV G LEVEL

```

0167      340 DD 350 J=1,B
0168      350 A(I,J)=C
0169      J=0
0170      DO 2 I=1,MM
0171      11=1-1
0172      IF(1-EQ.1) GO TO 7
0173      IF(GO(11).GT.8L(11)) GO TO 2
0174      J=J+1
0175      ICC=1
0176      L=0
0177      DJ 3 K=1,IP
0178      IF(1C(K).NE.0) GO TO 3
0179      L=L+1
0180      A(J,L)=DK(J,K)
0181      CONTINUE
0182      DO 10 K=1,IP
0183      IF(1B(K).NE.0) GO TO 10
0184      L=L+1
0185      A(J,L)=-DK(J,K)
0186      CONTINUE
0187      N=L+1
0188      IF(J-EQ.1) GO TO 2
0189      A(J,N)=0.
0190      CONTINUE
0191      A(1,N)=1.
0192      JA=J+1
0193      DO 8 I=1,L
0194      J=J+1
0195      A(J,I)=1.0
0196      M=J
0197      A(N+1,N)=1.0
0198      B=J+N+1
0199      B8=B+1
0200      DO 9 I=JA,M
0201      A(I,B)=1.0
0202      L=M
0203      DO 510 I=1,M
0204      A(N+1,I)=FLOAT(Z1+A(N+1,I))
0205      M=J
0206      NN=6
0207      CALL LINPRO(K2)
0208      IF(K2-EQ.0) V=V/2
0209      IF(K2-EQ.0) GO TO 1
0210      LL=M+1
0211      DO 1460 I=1,LL
0212      J=A(1,8B)
0213      SSS(J)=A(1,B)
0214      CONTINUE
0215      L=U
0216      DO 19 I=1,IP
0217      IF(1C(I).NE.0) GO TO 12
0218      L=L+1
0219      SSS(I)=SSS(L)
0220      GO TO 19
0221      SSS(I)=0
0222      CONTINUE

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OPT2

FORTRAN IV G LEVEL 21

```

0223 DD 13 I=1,IP
0224 IF(18(1).NE.0)GO TO 13
0225 L=L+1
0226 SS(1)=SS(1)-SSS(L)
0227 CONTINUE
0228 SUM=0.0
0229 DD 115 I=1,IP
0230 SUM=SUM+SS(1)*SS(1)
0231 SUM=DSQRT(SUM)
0232 IF(SUM.EQ.0.)GO TO 1101
0233 GO TO 1150
0234 LI=1
0235 IF(1XYZ.EQ.4) GO TO 3001
0236 RETURN
0237 DD 16 I=1,IP
0238 SS(1)=V*SS(1)/SUM
0239 DD 161 I=1,IP
0240 D(1)=XB(1,1)+SS(1)
0241 CONTINUE
0242 JIQ=0
0243 IAJ=0
0244 OBJ=OBJ(0)
0245 OFB=OBJ-FB(JJ)
0246 IF(OBJ.LT.FB(JJ)) GO TO 1180
0247 IF(1XYZ.EQ.4) GO TO 3001
0248 IF(17JUMP.EQ.1) GO TO 1123
0249 V=V/2.
0250 AXI=2.*AXI
0251 CU 108 I=1,JP
0252 BL(1)=BL(1)/2.
0253 LI=1
0254 IF(V.LT.VI) GO TO 1003
0255 IF(V.LT.AMIN) GO TO 1003
0256 FUPT=FB(1)
0257 DU 106 I=1,IP
0258 D(1)=XB(1,1)
0259 DD 107 J=1,JP
0260 GO(J)=GB(J)
0261 GO TO 101
0262 DD 1002 I=1,IP
0263 SS(1)=0.5*SS(1)
0264 GO TO 1001
0265 IF(1XYZ.EQ.4) RETURN
0266 DD 1182 I=1,IP
0267 D(1)=XB(1,1)
0268 CU 1004 J=1,JP
0269 GO(J)=GB(J)
0270 LI=0
0271 FUPT=FB(1)
0272 RETURN
0273 IF(SF(1).EQ.0.) JK=2
0274 IF(SE(1).EQ.0.) RETURN
0275 DD 154 I=1,IP
0276 D(1)=DT(1)-DK(1,1)*V
0277 CBJ=OBJ(0)
0278 IF(OBJ.LT.FB(JJ)) GO TO 102

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UPT2

FCRTRAN IV G LEVEL 21

```

0279 V=V/2.
0280 IF (V.LT.VT) RETURN
0281 IF (V.GT.AMIN) GO TO 153
0282 RETURN
0283 JK=0
0284 RETURN
0285 102
0286 1160
0287 IF (XYZ.EQ.4) JK=0
0288 IF (XYZ.EQ.4) RETURN
0289 CALL COMMOV(100,FGPT)
0290 IF (100.EQ.1) GO TO 118
0291 GO TO 1
0292 FGPT=FB(JJ)
0293 DO 1124 J=1,JP
0294 GO(J)=CB(J)
0295 DO 1125 I=1,IP
0296 D(I)=XB(I,JJ)
0297 GO TO 1
      END

```



```

0001 SUBROUTINE COMMON(100,EDPT)
0002 IMPLICIT REAL*8(A-F,H-Z)
0003 COMMON D(10),P(100),DL(10),DU(10),DZ(10),V,XB(10,5),GD(10),FB(5),
0004 CA(55,66),Q,IP,KP,JP,IA(10),KL, IDIM(11),
0005 COMMON IXJ
0006 COMMON/ZE/GS,GSS,SE(10),DK(11,10),DT(10),DI,SKAL,JIN,K,MU,
0007 C1H,JJ,J12,L11
0008 COMMON/POL/G8(10)
0009 COMMON/DOL/STEST,TDIF,AXI,AMIN,BL(10),AD,IN
0010 COMMON/PAT/DBJJ,K,IAYZ
0011 COMMON/CON/SS(10),BASE,IJ(10),JI(10),J1Q,I2JUMP
0012 DIMENSION GG(10),X(10)
0013 DO 1670 I=1,JP
0014   GG(I)=GG(I)
0015   IF(GG(I).GT.0.) GO TO 1660
0016   IF(GG(I).GT.BL(I)) GO TO 168
0017   CONTINUE
0018   NU=0
0019   GO TO 1731
0020   1698 IAJ=0
0021   DO 169 I=2,JIN
0022     KI=JI(I)
0023     GO(KI)=DBJJ(KI)
0024     GG(KI)=GD(KI)
0025   CONTINUE
0026   1731 CONTINUE
0027   JUB=0
0028   JQC=0
0029   GPP=1000000
0030   DO 120 M=2,JIN
0031     KK=JI(M)
0032     J=IJ(KK)
0033     SUM=0
0034     IF(GD(KK).GT.0) GO TO 1732
0035     GO TO 1735
0036     DO 1734 I=1,IP
0037       SUM=SUM+DK(I,I)*DK(J,I)
0038       IF(SUM.GT.0) GO TO 120
0039     JUB=JUB+1
0040     GP=GD(KK)/SE(J)
0041     IF(GP.GT.GPP) GU TO 120
0042     GPP=GP
0043     KPP=KK
0044     JPP=J
0045     CONTINUE
0046     IF(JUB.GT.0) GO TO 1737
0047     IF(JJ.GE.2) GO TO 1767
0048     JJ=JJ+1
0049     DO 31 I=1,IP
0050       SS(I)=2.*SS(I)
0051       XB(I,JJ)=D(I)
0052       D(I)=D(I)+SS(I)
0053       FB(JJ)=DBJJ
0054       IAJ=0
0055       DO 313 I=1,JP

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0055 CG 314 J=2,JIN
0056 K=J(IJ)
0057 IF(I.EQ.K) GO TO 313
0058 CONTINUE
0059 GU(I)=GB(J(I))
0060 GB(I)=GU(I)
0061 IZJUMP=1
0062 IOU=1
0063 RETURN
0064 CONTINUE
0065 K=JPP
0066 NU=KPP
0067 GS=GO(NU)
0068 IF(DARS(GS).LE..000001) GO TO 1767
0069 JUMP=0
0070 MU=NU
0071 CALL ZERO(JUMP)
0072 IF(SMAL.EQ.0) GO TO 310
0073 FOPT=FB(JJ)
0074 DO 311 I=1,JP
0075 D(I)=XB(I,JJ)
0076 DO 312 J=1,JP
0077 GO(J)=GB(J)
0078 IOU=2
0079 RETURN
0080 IF(J20.EQ.1.AND.JUMP.NE.2) J10=1
0081 IF(JUMP.NE.2) GO TO 1632
0082 GO TO 1698
0083 CONTINUE
0084 J1=0
0085 IXJ=0
0086 DO 1634 I=2,JIN
0087 K=J(I)
0088 IF(J30.GT.0) GO TO 1633
0089 GG(K)=GB(J(K))
0090 GO(K)=GG(K)
0091 IF(GG(K).LT.(-.000001)) J1=J1+1
0092 CONTINUE
0093 IF(J1.GT.0) GO TO 130
0094 J2=0
0095 IXJ=0
0096 DO 1630 I=1,JP
0097 DO 1636 J=2,JIN
0098 K=J(IJ)
0099 IF(I.EQ.K) GO TO 1630
0100 CONTINUE
0101 IF(J30.GT.0) GO TO 1631
0102 GG(I)=GB(J(I))
0103 GU(I)=GG(I)
0104 IF(GU(I).LT.(-.000001)) J2=J2+1
0105 CONTINUE
0106 J3C=0
0107 IF(J2.NE.0) GO TO 1773
0108 CEJ=GBJ(O)
0109 FOPT=OBJ
0110 IF(J10.EQ.1) IOU=2
  
```

```

0111 IF(J1Q-EQ-1) RETURN
0112 IF(JUMP-EQ-2) GO TO 1800
0113 GO TO 1766
0114 DO 1801 I=1,IP
0115 XB(1,1)=XB(1,JJ)
0116 FB(1)=FB(JJ)
0117 JJ=1
0118 GO TO 1766
0119 CS=CG(NU)
0120 MU=NU
0121 DO 1765 I=1,JP
0122 IF(CG(I)-GE-GS) GO TO 1765
0123 GS=CG(I)
0124 MU=I
0125 CONTINUE
0126 IF(MU-NE-NU) GO TO 1764
0127 JJ=JJ+1
0128 IF(JJ-LE-5) GO TO 1641
0129 DO 1642 I=1,IP
0130 XB(1,1)=XB(1,3)
0131 XB(1,2)=XB(1,4)
0132 XB(1,3)=XB(1,5)
0133 FB(1)=FB(3)
0134 FB(2)=FB(4)
0135 FB(3)=FB(5)
0136 JJ=4
0137 DO 1641 I=1,IP
0138 XB(1,JJ)=D(I)
0139 FB(JJ)=DBJ
0140 JW=JJ-1
0141 IF(FB(JJ)-GT-FB(JN)) GO TO 1760
0142 BASE=BASE+1
0143 ICC=0
0144 DO 1640 J=1,JP
0145 GB(J)=GG(J)
0146 CONTINUE
0147 IF(J1Q) 165,165,119
0148 IOU=1
0149 RETURN
0150 DO 1771 I=1,IP
0151 D(I)=XB(1,JW)
0152 FOPT=FB(JN)
0153 DO 1772 J=1,JP
0154 CU(J)=CE(J)
0155 IOU=2
0156 RETURN
0157 IF(JJ-GT-2) GO TO 112
0158 SUM=0.
0159 DO 1131 I=1,IP
0160 DC=XB(1,2)-XB(1,1)
0161 SUM=SUM+DC**2
0162 D(I)=XB(1,2)+DC
0163 SUM=DSORT(SUM)
0164 IF(SUM-LT-V/10.) GO TO 1123
0165 GO TO 1181
0166 JM=JJ-2

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CONMOV

FCATRAM IV G LEVEL 21

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0167 SUM=0.
0168 DO 114 I=1,IP
0169 CC=X8(I,JJ)-X8(I,JM)
0170 IF(OC.EQ.0) GO TO 114
0171 SUM=SUM+CC**2
0172 IF(J2Q.EQ.1) DC=(OC*V)/DABS(DC)
0173 C(I)=X8(I,JJ)+DC
0174 SUM=DSORT(SUM)
0175 IF(SUM.LT.V/10.1) GO TO 1123
0176 DO 1040 I=1,IP
0177 IF(D(I).LT.DL(I)) D(I)=DL(I)
0178 IF(D(I).GT.DU(I)) D(I)=DU(I)
0179 IF(J2Q.NF.1) GO TO 1698
0180 DO 1612 I=1,IP
0181 X8(I,1)=X8(I,JJ)
0182 JJ=1
0183 GO TO 1698
0184 DO 173 M=1,IP
0185 DTT(M)=D(M)
0186 X(M)=D(M)
0187 D(M)=X8(M,JJ)
0188 DT(M)=D(M)
0189 GS=GO(I)
0190 GG(I)=GG(I)
0191 MU=1
0192 BL(I)=2.*BL(I)
0193 JJ=2
0194 LI=2
0195 IF(DABS(GS).LE..000001)GO TO 1632
0196 GSS=GG(I)
0197 DO 174 M=1,IP
0198 D(M)=X(M)
0199 IF(DABS(GSS).LE..000001)GO TO 1632
0200 IU=0
0201 X1=DAES(GSS-GS)
0202 X2=DLGS(X1)+1
0203 IH=5+IDINT(X2/-69314718)
0204 JUMP=1
0205 MU=NU
0206 LI=LI
0207 CALL ZERO(JUMP)
0208 MU=0
0209 GO TO 172
0210 IU=0
0211 GSS=GG(MU)
0212 JACK=1
0213 IF(DABS(GSS).LE..000001)GO TO 1679
0214 DO 1768 I=1,IP
0215 DTT(I)=D(I)
0216 C(I)=X8(I,JJ)
0217 DT(I)=D(I)
0218 GS=GB(MU)
0219 JACK=2
0220 IF(DABS(GS).LE..000001)GO TO 1679
0221 JACK=0
0222 X1=DABS(GSS-GS)

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```

0223 X2=DLQC(X1)+1.
0224 IM=5+IDINT(X2/.69314718)
0225 CONTINUE
1861 T=GS/GS-GSS)
0226 DU 1769 I=1,IP
0227 D(1)=DT(1)+T*(DTT(1)-DT(I))
0228 IF(D(1)-LT-DL(I)) D(1)=DL(I)
0229 IF(D(1)-GT-DU(I)) D(1)=DU(I)
1769 IXJ=0
0231 GO(MU)=DBJ(MU)
0232 GG(MU)=GO(MU)
0233 IF(ABS(GO(MU)).GT..000001) GO TO 1689
0234 GO TO 1679
0235 GS=GSS
1689 GSS=GO(MU)
0237 IF(GS-LT-O) GO TO 1503
0238 GO TO 1504
0239 IF(GSS-LT-GS) GO TO 1610
0240 GO TO 1505
0241 IF(GSS-GT-GS) GO TO 1610
0242 IU=IU+1
0243 IF(IU-GT-IM) GO TO 1610
0244 DU 1676 I=1,IP
0245 DT(1)=DTT(1)
0246 DTT(1)=D(I)
0247 GO TO 1661
0248 IF(IJ-EQ-JU) DI=D1+2.
0249 IF(IJ-GT-2) GO TO 1615
0250 DO 1619 I=1,IP
0251 D(1)=XB(1,2)+(XB(1,2)-XB(I,1))/DI
1619 GO TO 1618
0253 JM=JJ-2
1615 DO 162 I=1,IP
0255 D(1)=XB(1,JJ)+(XB(I,JJ)-XB(I,JM))/DI
162 JU=JJ
0257 DO 1616 I=1,IP
0258 IF(D(1)-LT-DL(I)) D(1)=DL(I)
0259 IF(D(1)-GT-DU(I)) D(1)=DU(I)
1616 IF(I-EQ-3) GO TO 1698
0261 DBJ=08J(I)
1679 IF(DBJ-GT-F8(JJ)) GO TO 1123
0263 IF(JACK-EQ-1) GO TO 1707
0264 IF(JACK-EQ-2) GO TO 1123
0265 DO 1677 I=1,JP
0266 IF(I-EQ-MJ) GO TO 1677
0267 GO(1)=08J(1)
0268 GG(1)=GO(1)
0269 CONTINUE
1677 CONTINUE
1707 JU=0
0272 DO 1121 J=1,JP
0273 IF(GO(J).LT..000001) JO=JG+1
0274 CONTINUE
1121 IF(JO-LE-O) GO TO 1122
0275 J3G=1
0276 J2Q=1
0277 J2Q=1
0278

```

```

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0279      GO TO 1632
0280      LI=2
0281      IXJ=0
0282      FORT=08J(0)
0283      ICU=2
0284      RETURN
0285      FORT=F8(JJ)
0286      DO 1124 J=1,JP
0287      GO(J)=GB(J)
0288      DO 1125 I=1,IP
0289      D(I)=XB(I,JJ)
0290      ICU=2
0291      RETURN
0292      END

```



```

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0001 SUBROUTINE ZERO(JUMP)
0002 IMPLICIT REAL*8(A-H,O-Z)
0003 COMMON D(10),P(100),DL(10),DU(10),DZ(10),V,XB(10,5),GO(10),FB(5),
0004 CA(55,66),O,IP,IDUM(24)
0005 COMMON IXJ
0006 COMMON/ZE/GS,GSS,SE(10),DK(11,10),DT(10),DIT(10),D1,SHAL,JIN,K,NU,
0007 CIN,JJ,J12,LI
0008 DIMENSION GG(10)
0009 IU=0
0010 IF(JUMP.EQ.1) GO TO 175
0011 SHAL=0
0012 KU=0
0013 CONTINUE
0014 DO 1740 I=1,IP
0015 DT(I)=D(I)
0016 DT(I)=DT(I)+DK(K,I)*GS/SE(K)
0017 CONTINUE
0018 DO 1032 I=1,IP
0019 IF(D(I).LT.DL(I)) D(I)=DL(I)
0020 IF(D(I).GT.DU(I)) D(I)=DU(I)
0021 DIT(I)=D(I)
0022 IAJ=0
0023 GSS=OBJ(NU)
0024 IF(GS.LT.O.) GO TO 1701
0025 GO TO 1702
0026 IF(GSS.LT.GS) GO TO 1703
0027 GO TO 1704
0028 IF(GSS.GT.GS) GO TO 1703
0029 GO TO 1704
0030 IF(KU.LE.O) GO TO 1713
0031 GO TO 1710
0032 DO 1705 I=1,IP
0033 D(I)=DT(I)
0034 CALL DB(KU,LI)
0035 SUM4=0.
0036 J=K
0037 DO 1706 I=1,IP
0038 CK(J,I)=DZ(I)
0039 SUM4=SUM4+DZ(I)*2
0040 SUM4=DSORT(SUM4)
0041 SE(J)=SUM4
0042 DO 1707 I=1,IP
0043 DK(J,I)=-DK(J,I)/SUM4
0044 KU=1
0045 GO TO 1738
0046 IF(DABS(GSS)-LF-.000001) GO TO 1632
0047 X1=DA2(GSS-GS)
0048 X2=DL0G(X1)+1.
0049 IN=5+IDINT(X2/.69314718)
0050 IU=0
0051 CONTINUE
0052 T=GS/(GS-GSS)
0053 DO 163 I=1,IP
0054 D(I)=DT(I)+T*(DIT(I)-DT(I))
0055 CONTINUE
0056 DO 160 I=1,IP

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ZERO

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0055 IF(D(1)-LT.DL(1)) D(1)=DL(1)
0056 IF(D(1)-GT.DU(1)) D(1)=DU(1)
0057 IXJ=0
0058 GG(NU)=OBJ(NU)
0059 IF(DABS(GG(NU))-GT-.000001) GO TO 1601
0060 GU TO 1632
0061 GS=GS5
0062 GSS=GG(NU)
0063 IF(GS-LT.0) GO TO 1603
0064 GU TO 1604
0065 IF(GSS-LT.GS) GO TO 1710
0066 GU TO 1605
0067 IF(GSS-GT.GS) GO TO 1710
0068 IU=IU+1
0069 IF(IU-GT.IM) GO TO 1710
0070 DU 1602 L=1,IP
0071 DT(L)=DT(L)
0072 DT(L)=D(L)
0073 GU TO 1600
0074 IF(JJ.EQ.J12) DI=2.0DI
0075 SAN=D.
0076 IF(JJ-GT.2) GO TO 1715
0077 IF(JJ-EQ.2) GO TO 1100
0078 DO 1200 I=1,IP
0079 XB(I,2)=D(I)
0080 DO 1719 I=1,IP
0081 CX=XB(I,2)-XB(I,1)
0082 SAN=SAN+DX**2
0083 D(I)=XB(I,2)+DX/DI
0084 SAN=DSORT(SAN)
0085 SAN=SAN/DI
0086 IF(SAN-LT-V) GO TO 1
0087 GU TO 1716
0088 JM=JJ-2
0089 DO 172 I=1,IP
0090 DX=XB(I,JJ)-XB(I,JM)
0091 SAN=SAN+DX**2
0092 D(I)=XB(I,JJ)+DX/DI
0093 SAN=DSORT(SAN)
0094 SAN=SAN/DI
0095 IF(SAN-LT-V) GO TO 1
0096 DO 1716 I=1,IP
0097 IF(D(1)-LT.DL(1)) D(1)=DL(1)
0098 IF(D(1)-GT.DU(1)) D(1)=DU(1)
0099 J12=JJ
0100 JUMP=2
0101 RETURN
0102 SMAL=1
0103 RETURN
0104 END

```

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```

0001 SUBROUTINE LINPRO(K2)
0002 IMPLICIT REAL*8(A-H,O-Z)
0003 INTEGER Z,E,G,BB,M,B,R,C,H
0004 COMMON D(1C),U(100),OL(10),OU(10),OZ(10),V,XB(10,5),CH(10),FB(5),
0005 CA(55,66),Q,IP,KP,JP,JA(10),KL,KM,N,M,L,B,BB,E,G,Z,H,W
0006 COMMON IXJ
0007 K2=1
0008 NN=6
0009 M=M-1.0
0010 LL=M+2
0011 DO 560 K=2,LL
0012 A(K-1,M+G+K-1)=1
0013 A(K-1,BB)=K+N+G-1
0014 IF(G-WE-0) GO TO 620
0015 IF(E-EQ-0) GO TO 780
0016 GO TO 650
0017 KK=L+E+2
0018 LL=M+2
0019 DO 630 K=KK,LL
0020 A(K-1,M+N-L-E-1)=-1
0021 Q=0
0022 LL=N+G
0023 DO 760 J=1,LL
0024 S=0
0025 LL=M-G-E+2
0026 KK1=M+1
0027 DO 700 I=LL1,KK1
0028 S=S+A(I,J)
0029 A(M+1,J)=-S
0030 IF(A(M+1,J).GT.0) GO TO 760
0031 Q=A(M+1,J)
0032 C=J
0033 CONTINUE
0034 S=0
0035 LL=M-G-E+2
0036 KK=M+1
0037 DO 763 J=LL,KK
0038 S=S+A(J,B)
0039 A(M+1,B)=-S
0040 CONTINUE
0041 IF(G-EQ-0) GO TO 810
0042 LL=N+1
0043 KK=M+G
0044 IF(L-EQ-0) GO TO 830
0045 LL=N+G+1
0046 KK=N+G+L
0047 IU=1
0048 IF(G+E-EQ-0) GO TO 2000
0049 LL=N+G+L+1
0050 KK=B-1
0051 IQ=1
0052 GO TO 2000
0053 IF(Q-EQ-99999) GO TO 1230
0054 IF(Q-EQ-0) GO TO 1330
0055 GO TO 1400

```



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LINPRO

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0056 920 H=M+1
0057 930 Q=-1E39
0058 940 R=-1
0059 LL=M+1
0060 950 DO 1000 I=1,LL
0061 960 IF(A(I,C)-LE-0) GO TO 1000
0062 970 IF(A(I,B)/A(I,C)-GT-0) GO TO 1000
0063 980 Q=A(I,B)/A(I,C)
0064 990 R=1
0065 1000 CONTINUE
0066 1010 IF(DFLOAT(R)-GE--5) GO TO 1050
0067 1020 IQ=2
0068 1030 GO TO 2000
0069 1050 P=A(R,C)
0070 1060 A(R,B)=C
0071 1070 DO 1080 J=1,B
0072 1080 A(R,J)=A(R,J)/P
0073 LL=M+1
0074 1100 DO 1180 I=1,LL
0075 1110 IF(I-EQ-K) GO TO 1180
0076 1120 DO 1170 J=1,B
0077 1130 IF(J-EQ-C) GO TO 1170
0078 1140 A(I,J)=A(I,J)-A(R,J)*A(I,C)
0079 1150 IF(DABS(A(I,J))-GT-.1E-4) GO TO 1170
0080 1160 A(I,J)=0
0081 1170 CONTINUE
0082 1180 CONTINUE
0083 LL=M+1
0084 1190 DO 1200 I=1,LL
0085 1200 A(I,C)=0
0086 1210 CONTINUE
0087 1220 A(R,C)=1
0088 1230 Q=0
0089 1240 LL=M+G+L
0090 1250 IF(A(M+1,J)-GT-.01G) GO TO 1280
0091 1260 Q=A(M+1,J)
0092 1270 C=J
0093 CONTINUE
0094 1280 GO TO 900
0095 1290 IF(W-EQ-M+1) GO TO 1360
0096 1300 W=N-1
0097 1310 IF(A(M+2,B)-LT-.1E-5) GO TO 1353
0098 1320 K2=C
0099 1330 RETURN
0100 1340 LL=M+1
0101 1350 DO 1358 I=1,LL
0102 1358 IF(POINT(A(I,BB))-LE-N+G+L) GO TO 1358
0103 1355 DO 1356 J=1,B
0104 1356 A(I,J)=0
0105 1358 CONTINUE
0106 1359 GO TO 1230
0107 1360 CONTINUE
0108 1400 IF(C-EQ-0) GO TO 1420
0109 1420 LL=M+1
0110 1430 DO 1460 I=1,LL

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LINPRO

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```

0112      1440  IF(I0INT(A(1,88)),EQ,0) GO TO 1460
0113      1460  CONTINUE
0114      1470  IF(G-NE,0) GO TO 920
0115      1520  KK=N+1
0116      LL=B-G-1
0117      XJJ=-2*A(N+1,8)
0118      LL=H-1
0119      IQ=3
0120      1550  GO TO 2000
0121      2000  LL=H-1
0122      LL=X+1
0123      GO TO(895,1050,999),IQ
0124      999   RETURN
0125      END

```

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PATRN

FURTRAN IV 6 LEVEL 21

```

0001 SUBROUTINE PATRN(KH,SB)
0002 IMPLICIT REAL*8(A-H,O-Z)
0003 COMMON D(10),F(100),CL(10),DU(10),OZ(10),A,XB(10,5),C(10),FB(5),
0004 CV(55,66),Q,IP,KP,JP,LDUN(22)
0005 COMMON IXJ
0006 COMMON/FIN/X(10),CK(10),IA(10),IK,IL,IC(10)
0007 COMMON/PAT/ST,JK,IXYZ
0008 COMMON/BAS/IK1,IK2
0009 DIMENSION AD(10,10),EI(10,10),ET(10,10),AZ(10),IX(10)
0010 IXYZ=4
0011 AMIN=-.0000001
0012 IK1=0
0013 IK2=0
0014 LI=2
0015 DI=10.*A
0016 TDIF=10.E+10
0017 IPP=1P
0018 AL=A
0019 IM=0
0020 STEST=0.
0021 KA=0
0022 KW=0
0023 KT=0
0024 KL=0
0025 KF=0
0026 DO 111 K=1,IPP
0027 IF(D(K)-LT.OL(K))D(K)=OL(K)
0028 IF(D(K)-GT.DU(K))D(K)=DU(K)
0029 111 X(K)=D(K)
0030 25 KK=1
0031 DO 1 K=1,IPP
0032 DO 22 I=1,IPP
0033 EI(I,K)=0.
0034 EI(I,K)=0.
0035 EI(K,K)=1.
0036 EI(K,K)=1.
0037 1 CONTINUE
0038 ST=SB
0039 IF(KA-EQ.1)GO TO 9
0040 KA=1
0041 IK=0
0042 CALL FIND(SB,1)
0043 IF(I.NE.0) GO TO 1000
0044 9 ST=SB
0045 GO TO 100
0046 IK=0
0047 CALL FIND(ST,1)
0048 IF(I.NE.0) GO TO 1000
0049 100 KL=KL+1
0050 IK=1
0051 KF=KF+1
0052 DO 2 J=1,IPP
0053 DO 17 K=1,IPP
0054 AZ(K)=EI(J,K)*A
0055 IF(IK.NE.0) AZ(K)=EI(J,K)*A

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PATRN

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```

0056 17 D(K)=D(K)+AZ(K)
0057 DO 35 K=1,IPP
0058 IF(D(K).GT.DU(K))GO TO 4
0059 IF(D(K).LT.DL(K))GO TO 4
0060 35 CONTINUE
0061 CALL FIND(SA,I)
0062 IF(I.NE.O) GO TO 1000
0063 IF((ST-SA)/DABS(SB).GT.2.E-16) GO TO 5
0064 4 DO 18 K=1,IPP
0065 D(K)=D(K)-AZ(K)-AZ(K)
0066 DO 36 K=1,IPP
0067 IF(D(K).LT.DL(K))GO TO 3
0068 IF(D(K).GT.DU(K))GO TO 3
0069 36 CONTINUE
0070 CALL FIND(SA,I)
0071 IF((ST-SA)/DABS(SB).LT.2.E-16) GO TO 3
0072 5 ST=SA
0073 GO TO 2
0074 3 DO 21 K=1,IPP
0075 D(K)=D(K)+AZ(K)
0076 2 CONTINUE
0077 IF((SB-ST)/DABS(SB).LT.2.E-16) GO TO 7
0078 26 SUM=0.
0079 IN=0
0080 KX=0
0081 DO 8 K=1,IPP
0082 IX(K)=0
0083 D1=2.*D(K)-X(K)
0084 AD(1,K)=D(K)-X(K)
0085 DX=X(K)
0086 IF(DX.EQ.O.) DX=1.
0087 IF(UABS(AD(1,K)/DX).LT.1.E-15) GO TO 88
0088 IX(K)=1
0089 KX=KX+1
0090 SUM=SUM+AD(1,K)*AD(1,K)
0091 X(K)=D(K)
0092 IF(D1.LT.DL(K))D1=DL(K)
0093 IF(D1.GT.DU(K))D1=DU(K)
0094 D(K)=D1
0095 SB=ST
0096 SUM=DSQRT(SUM)
0097 IF(SUM.LT.A*.5) GO TO 7
0098 KK=0
0099 DO 11 K=1,IP
0100 ET(1,K)=EI(1,K)
0101 DX=X(K)
0102 IF(DX.EQ.O.) DX=1.
0103 IF(DABS(AD(1,K)/DX).LT.1.E-15) AD(1,K)=0.
0104 EI(1,K)=AD(1,K)/SUM
0105 DO 12 I=2,IP
0106 CU 12 J=1,IP
0107 ET(I,J)=EI(1,J)
0108 ET(I,J)=0.
0109 AD(I,J)=0.
0110 K=1
0111 DO 13 I=1,IP

```

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PATRN

```

0112 IF(IX(1)-EQ.0) GO TO 13
0113 M=I+1
0114 IF(M-GT-IP) GO TO 89
0115 K=K+1
0116 L=K-1
0117 SUMA=0
0118 DO 14 J=M,IP
0119 AD(K,J)=AD(I,J)
0120 SUMA=SUMA+EI(L,J)+AD(K,J)
0121 SUM=0
0122 DO 15 J=1,IP
0123 EI(K,J)=AD(K,J)-EI(L,J)+SUMA
0124 IF(DABS(EI(K,J)).LE.1.E-35) GO TO 15
0125 SUM=SUM+EI(K,J)+2
0126 CONTINUE
0127 IF(SUM-LT-1.E-32) GO TO 13
0128 SUM=DSORT(SUM)
0129 DO 16 J=1,IP
0130 DX=X(K)
0131 IF(DX.EQ.0.) DX=1.
0132 IF(DABS(EI(K,J)/DX).LT.1.E-15) EI(K,J)=0.
0133 EI(K,J)=EI(K,J)/SUM
0134 CONTINUE
0135 J=KX
0136 DO 180 I=1,IP
0137 IF(IX(1)-EQ.1) GO TO 180
0138 J=J+1
0139 EI(J,I)=1.
0140 CONTINUE
0141 GO TO 19
0142 7 DO 20 K=1,IPP
0143 D(K)=X(K)
0144 IF(KK)25,24,23
0145 KK=-1
0146 IF(KF-GT-200)GO TO 23
0147 GO TO 9
0148 CONTINUE
0149 LI=2
0150 TN=58
0151 IF(KL-GT-KT+4) GO TO 33
0152 A=A/2.
0153 CALL OPT2(SE,LI)
0154 PRINT 1500,A,SB,ST,(D(I),I=1,IP)
0155 FORMAT('CHECK POINT A=',F10.5,'SB=',F16.8,'ST=',F16.8,'D=',5F12
1.7)
KT=KL
0156 IF(JK-EQ.2) KN=1
0157 IF(JK-EQ.2) GO TO 1001
0158 KF=0
0159 IF(JK-NE-0) GO TO 40
0160 IF(A-EQ.AL) GO TO 20
0161 AL=A
0162 DIF=DABS((SB-STEST)/SB)
0163 IF(DIF-GT. 1.E-05) GO TO 45
0164 IM=IM+1
0165 IF(IM-LT-2) GO TO 150
0166

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C167  IF(DIF-GI-TDIF) GO TO 45
C168  GO TO 1001
C169  IM=J
C170  SIEST=SB
C171  TDIF=0IF
C172  GO TO 26
C173  IM=J
C174  A=A/2.
C175  DO 47 K=1,IPP
C176  D(K)=X(K)
C177  IF(A-LT-AMIN) GO TO 1001
C178  GO TO 190
C179  A=A/2
C180  IF(A-LT-AMIN) GO TO 1001
C181  GO TO 149
C182  DO 1003 I=1,IP
C183  D(I)=X(I)
C184  KN=1
C185  RETURN
C186  DO 1002 I=1,IP
C167  D(I)=X(I)
C188  KN=0
C189  RETURN
C190  END

```



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FIND

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```

0001 SUBROUTINE FIND(TU,1)
0002 IMPLICIT REAL*8(A-H,O-Z)
0003 COMMON D(10),P(100),DL(10),DU(10),DZ(10),A,XB(10,5),G(10),FB(5),
0004 CV(55,66),Q,IP,KP,JP,LDUN(22)
0005 COMMON IXJ
0006 COMMON/FIN/X(10),CK(10),IA(10),IK,IL,IC(10)
0007 DIMENSION DT(10)
0008 LI=2
0009 I=0
0010 IXJ=0
0011 TD=DEJ(0)
0012 IF(JP-EQ-0) RETURN
0013 DO 25 K=1,1P
0014 DT(K)=0(K)
0015 IF(IK-EQ-0) GO TO 51
0016 IF(IL-EQ-0) RETURN
0017 DO 52 J=1,IL
0018 IB=IC(J)
0019 G(IB)=QB(J,IB)
0020 IF(G(IB)) 5,5,52
0021 I=I+1
0022 IA(I)=IB
0023 CONTINUE
0024 RETURN
0025 IL=0
0026 DO 3 J=1,JP
0027 G(J)=DEJ(J)
0028 IF(G(J)-GT. 01) GO TO 3
0029 IL=IL+1
0030 IC(IL)=J
0031 IF(G(J)) 4,4,3
0032 I=I+1
0033 IA(I)=J
0034 CONTINUE
0035 RETURN
0036 END

```

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GBJ

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```
0001 REAL FUNCTION UBJ8(KLX)  
0002 IMPLICIT REAL*8(A-H,O-Z)  
0003 COMMON D(10),P(100),DUM(3727),IDUM(25)  
0004 UBJ=8-U  
0005 IF(B-EQ-0.-OR-U-EQ-0.) RETURN  
0006 UBJ=(B-U)/DABS(U)  
0007 RETURN  
0008 END
```

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7. AUTHOR(s) <b>JACOB MORADI AND MICHAEL PAPPAS</b>	8. CONTRACT OR GRANT NUMBER(s) <b>ONR N00014-75-C-0987</b>	
9. PERFORMING ORGANIZATION NAME AND ADDRESS <b>NEW JERSEY INSTITUTE OF TECHNOLOGY 323 HIGH STREET NEWARK, NEW JERSEY 07102</b>	10. PROGRAM ELEMENT, PROJECT, TASK AREA & WORK UNIT NUMBERS <b>12 119 p.</b>	
11. CONTROLLING OFFICE NAME AND ADDRESS <b>DR. NICHOLAS PERRONE, (Code 474) OFFICE OF NAVAL RES., 800 NO. QUINCY ST. ARLINGTON, VIRGINIA 22203</b>	12. REPORT DATE <b>MARCH 77</b>	
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19. SUPPLEMENTARY NOTES		
20. KEY WORDS (Continue on reverse side if necessary and identify by block number)  <b>MATHEMATICAL PROGRAMMING; DESIGN, OPTIMAL, OPTIMIZATION, NUMERICAL, DESIGN, COMPUTER-AIDED</b>		
20. ABSTRACT (Continue on reverse side if necessary and identify by block number)  <b>A FAST SEARCH ALGORITHM FOR THE SOLUTION OF NONLINEAR MATHE- MATICAL PROGRAMMING OPTIMIZATION PROBLEMS IS PRESENTED IN THIS REPORT. THE PROCEDURE COMBINES A "BOUNDARY TRACKING" (BT) STRATEGY WITH THE FEASIBLE DIRECTION FINDING METHOD OF ZOUTENDIJK. THIS ALGORITHM WAS COMPARED WITH TWENTY OTHER CODES REPRESENTING MOST OF THE POPULAR NUMERICAL OPTIMIZATION METHODS ON TEN TEST PROBLEMS. THE NEW CODE PROVED SUPERIOR TO ALL OTHERS IN OVERALL GENERALITY AND EFFICIENCY.</b>		

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